

Lecture I

Phenomenon - part of reality that is subject of study.
Has form of independence and internal cohesion

e.g. Ball on Beld

Playing Chess.

Inverted pendulum on a cart.

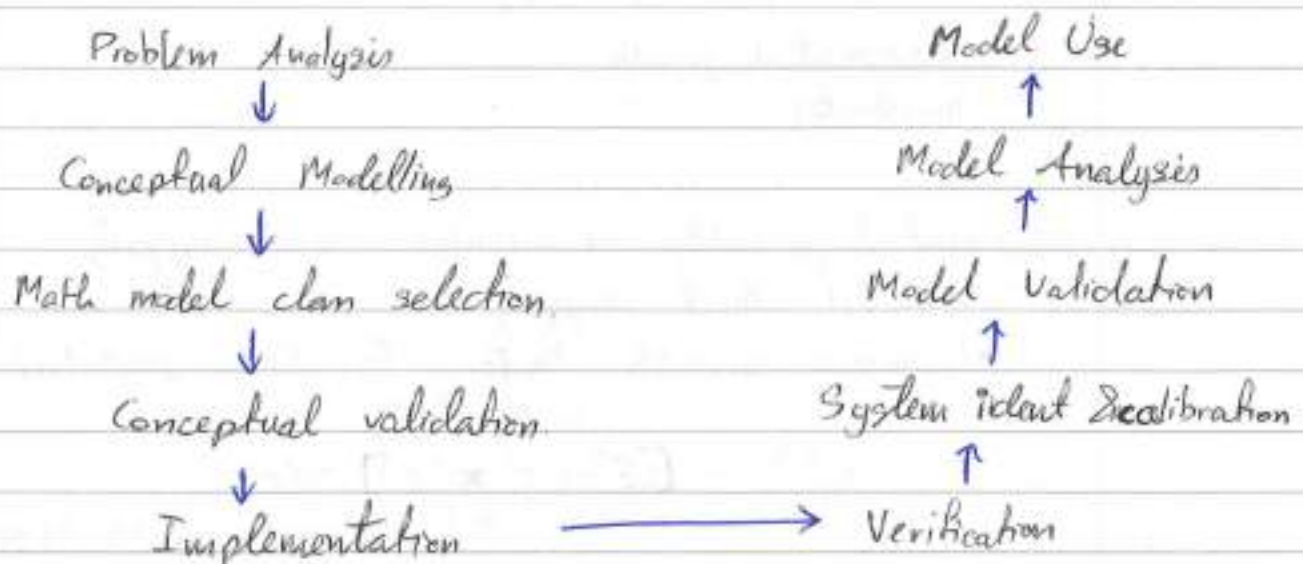
Model - abstract rep. of reality.

- always simplification of reality - not reality itself
- good model contains all structures & relationships that matter and ~~ignore~~ ^{leave out} all others of less relevance.

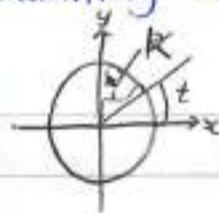
Math Model: relationships of phenomenon are represented by equation and ^{conditions on quantities} ~~corresponding values~~.

- correspondance rule gives them meaning.

Modelling Cycle - Ensure all parties consent
Hardly ever right the first time
Sometimes client doesn't know what they want.



Running on the Unit Circle



$$(x(t), y(t)) = K(\cos(t), \sin(t))$$

$$x'(t) = -K\sin(t)$$

$$y(t) = K\cos(t)$$

$$\dot{x} = -y$$

$$\dot{y} = x$$

$$\frac{dy}{dx} = \frac{-x}{y}$$

$$y dy = -x dx$$

Integrating:

$$\frac{1}{2} y^2 = -\frac{1}{2} x^2 + C$$

$$x^2 + y^2 = C$$

Lotka-Volterra models - which move onto predator-prey.

Sensitivity Analysis - influence of initial conditions/
parameters
- reliability of our model.

Growth of a population.

- growth depends on pop. size.

$$x'(t) = \text{growth factor} \cdot x(t)$$

- which kind of $x(t)$ solves this?

$$x(t) = e^{et} x_0$$

- exponential growth

- unrestricted.

Exponential growth w/ limited food supply.

- Limited food supply

- decrease growth factor for large populations

$$x'(t) = [(\text{growth factor}) - \sigma x(t)] x(t)$$

factor to reduce growth based on [pop.]

- if pop. is too large; negative growth
(starvation).

How to measure the parameters?

- Exponential growth factor E is easily observed directly in a small pop.
- σ can be measured in equilibrium stage, i.e. at $x'(t) = 0$.

Lotka-Volterra models

$$x'(t) = (E - \sigma x(t)) x(t)$$

$$x'(t) = (E - \sigma x(t)) \cdot x(t) = 0$$

$$x(t) = 0 \quad \text{or} \quad E - \sigma x(t) = 0$$

extinct

$$\Rightarrow \sigma = \frac{E}{x(t)} \quad \text{equilibrium}$$

Competing Species

- Two species fighting over shared limited food supply.
- Pop. of other species affects growth of the first.

two competing species

limit of growth of zebra by buffalo.
pop. of water buffalo

Zebras - $x'(t) = (E_1 - \sigma_1 x(t) - \alpha_1 y(t)) x(t)$

Buffalos - $y'(t) = (E_2 - \sigma_2 y(t) - \alpha_2 x(t)) y(t)$

equilibria.

$$\begin{cases} x'(t) = 0 \\ y'(t) = 0 \end{cases}$$

Cases for equilibria

$$\bullet x(t) = 0 \quad \wedge \quad y(t) = 0$$

$$\bullet x(t) = 0 \quad \wedge \quad E_2 - \sigma_2 y(t) - \alpha_2 x(t) = 0$$

$$\Rightarrow y(t) = \frac{E_2}{\sigma_2}$$

$$\bullet y(t) = 0 \quad \wedge \quad E_1 - \sigma_1 x(t) - \alpha_1 y(t) = 0$$

$$\Rightarrow x(t) = \frac{E_1}{\sigma_1}$$

$$\begin{cases} E_1 - \sigma_1 x(t) - \alpha_1 y(t) = 0 \\ E_2 - \sigma_2 y(t) - \alpha_2 x(t) = 0 \end{cases} \Rightarrow \begin{cases} x(t) = \frac{E_1 - \alpha_1 y(t)}{\sigma_1} \\ y(t) = \frac{E_2 - \alpha_2 x(t)}{\sigma_2} \end{cases}$$

Predator-Prey Models

- Prey pop. as before with possibly limited food.

- predator pop. that eat prey.

- predator pop. will starve if there are no prey.

Prey

Zebra

$$x'(t) = (e_1 - \sigma_1(x(t)) - \alpha_1 y(t)) x(t)$$

too many zebras this starve

$$= (e_1 x(t) - \sigma_1(x(t)) - \alpha_1 x(t) y(t))$$

known as Lotka-Volterra pop.

Predators

Lion

$$y'(t) = (-e_2 + \alpha_2 x(t) - \sigma_2 y(t)) y(t)$$

decreasing more zebras pop. if no zebras = lion can eat

too many lions will starve lion

$$= -e_2 y(t) + \alpha_2 x(t) y(t) - \sigma_2 (y^2(t))$$

Jacobian

classical w.r.t. x

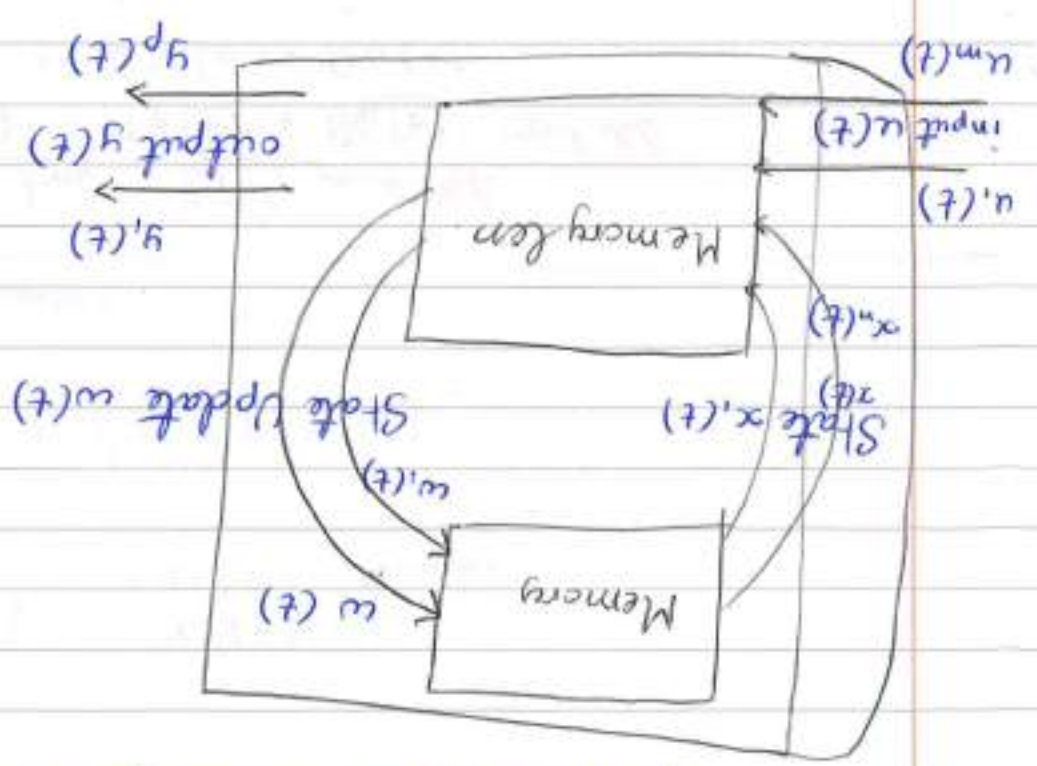
w.r.t. y

$$\begin{bmatrix} x'(t) \\ y'(t) \end{bmatrix} = \begin{bmatrix} e_1 - \sigma_1 x - \alpha_1 y \\ \alpha_2 x - e_2 - \sigma_2 y \end{bmatrix}$$

at (0,0) linearize this as

$$\begin{bmatrix} e_1 & 0 \\ 0 & e_2 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} e_1 & 0 \\ 0 & e_2 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix}$$

Mathematical Modeling Lecture 2.



output

$$y_p(t) = g(x_1(t), x_2(t), \dots, x_n(t), u_1(t), \dots, u_n(t), t)$$

it is also dependent on time!

$$x(t) = \begin{pmatrix} x_1(t) \\ \vdots \\ x_n(t) \end{pmatrix} = \text{vectorised}$$

$$y(t) = g(x(t), u(t), t)$$

$$u(t) = \begin{pmatrix} u_1(t) \\ \vdots \\ u_m(t) \end{pmatrix}$$

state update

His function is combined $x'(t)$ & $y'(t)$ of predator prey. state is for example the pop. of both. His combined pops. $f(x(t), u(t), t)$ discrete-time $w(t) = x[t+1]$ square bracket denote discrete. continuous-time $w(t) = x'(t)$.

if g and f are time-invariant? and linear.

$$y_p(t) = (c_1 x_1(t) + c_2 x_2(t) + \dots + c_n x_n(t) + d_1 u_1(t) + \dots + d_m u_m(t))$$

$$y(t) = Cx(t) + Du(t)$$

MIMO LTI

multi input - multi output linear time invariant.

$w(t)$ in continuous time.

$$\dot{x}(t) = A x(t) + B u(t)$$

$n \times m$ $n \times n$ $n \times m$

$$w(t) = \begin{pmatrix} x(t) \\ y(t) \end{pmatrix}$$

State Prey Predator

$$y(t) = (1 \ 1) w(t)$$

output.
(eg example Hawk counts total wildlife)

discrete-time LTI. *pop as state*

$$x[k+1] = A x[k] + B u[k] \quad \text{input state}$$

$$y[k] = C x[k] + D u[k]$$

CT (continuous time).

$$\dot{x}(t) = A x(t) + B u(t)$$

$$y(t) = C x(t) + D u(t)$$

Species Metamorphoses



$$\dot{x}_1(t) = -k_1 x_1(t)$$

$$\dot{x}_2(t) = k_1 x_1(t) - k_2 x_2(t)$$

$$\dot{x}_3(t) = k_2 x_2(t)$$

state $x(t)$

$x_1(t)$ = pop size A

$x_2(t)$ = pop size B

$x_3(t)$ = pop size C

$$x(t) = \begin{pmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{pmatrix}$$

$$\dot{x}(t) = \begin{pmatrix} -k_1 & 0 & 0 \\ k_1 & -k_2 & 0 \\ 0 & k_2 & 0 \end{pmatrix} x(t)$$

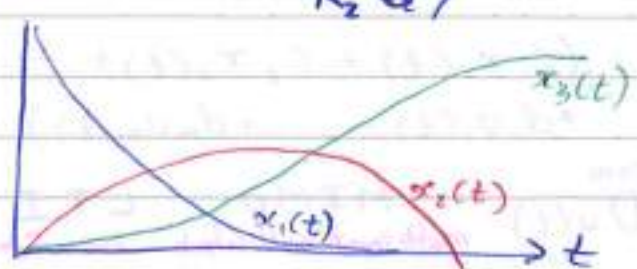
Total pop = $(1 \ 1 \ 1) x(t)$

$$\frac{d}{dt} (1^T x(t)) = 1^T \dot{x}(t)$$

column sum of A which = 0.

$= (1^T A) x(t) = 0$

Note: we have conservation of population.



$y(t) = (1 \ 1 \ 1) x(t)$ *one input*

$$\dot{x}(t) = \begin{pmatrix} -k_1 & 0 & 0 \\ k_1 & -k_2 & 0 \\ 0 & k_2 & 0 \end{pmatrix} x(t) + \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} u(t)$$

sum of column

$$\begin{aligned}
 x_1'(t) &= -k_1 x_1(t) + \mu(t) \quad \text{one from previous B. (birth of the eggs)} \\
 x_2'(t) &= k_1 x_1(t) + k_2 x_2(t) \\
 x_3'(t) &= k_2 x_2(t) - d x_3(t) \quad \text{death of the butterflies.}
 \end{aligned}$$

Markov Chains

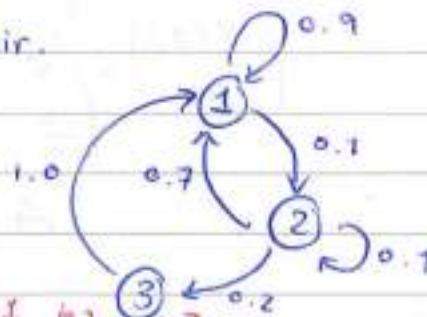
$Z(t) \in \{1, \dots, n\}$ random sequence

$$\text{Prob}(Z[t+1] = i | Z[t] = j) = \underline{P}_{ij}$$

$$p[t] = \begin{bmatrix} \text{Prob}(Z[t] = 1) \\ \vdots \\ \text{Prob}(Z[t] = n) \end{bmatrix}$$

Markov chain windows computer state

1. working
2. down
3. in repair.



$$\underline{P} = \begin{bmatrix} 0.9 & 0.7 & 1.0 \\ 0.1 & 0.1 & 0 \\ 0 & 0.2 & 0 \end{bmatrix}$$

$\downarrow$ if in 1
 $\downarrow$ to 2
 $\downarrow$ in 3

$$x[0] = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \quad (\text{working comp.})$$

$$x[k+1] = \underline{P} x[k]$$

$$\text{steady state} \quad x[k+1] = x[k]$$

$$\lambda \underline{1} x = \underline{P} x$$

$$P_x[k] = x[k]$$

$$(\underline{P} - \lambda \underline{I}) \underline{v} = 0 \quad \text{eigenvector.}$$

$$\begin{pmatrix} -0.1 & 0.7 & 1 \\ 0.1 & -0.9 & 0 \\ 0 & 0.2 & -1 \end{pmatrix} \underline{v} = 0 \sim \begin{pmatrix} 1 & 1 & 1 \\ 0 & 0.2 & -1 \\ 0.1 & -0.9 & 0 \end{pmatrix} \begin{matrix} 1 \\ 0 \\ 0 \end{matrix}$$

but this is linearly dependent
 get rid of top row then subrow sum to 1.
 but the prob must sum up to 1.

e.x. traffic lights.

red or green

if red, it will stay red w.p. $2/3$ and will

turn green w.p. $1/3$

if green, stay green w.p. $1/2$, turn red w.p. $1/2$

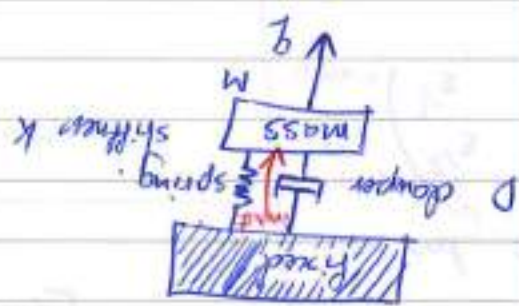
$$\text{start red. } x[0] = \begin{pmatrix} 1 \\ 0 \end{pmatrix}$$

$$\underline{P} = \begin{pmatrix} 2/3 & 1/2 \\ 1/3 & 1/2 \end{pmatrix}$$

red $\downarrow$
 green $\downarrow$

$$x[1] = \underline{P} x[0] = \begin{pmatrix} 2/3 \\ 1/3 \end{pmatrix}$$

$$\begin{aligned}
 x[2] &= \underline{P} x[1] = \underline{P}^2 x[0] \\
 &= \begin{pmatrix} (2/3)^2 + 1/6 \\ 2/9 + 1/6 \end{pmatrix} = \underline{P} \underline{P} x[0]
 \end{aligned}$$



mass-damper-spring

$$x(t) = \begin{pmatrix} q(t) \\ \dot{q}(t) \end{pmatrix}$$

$$\dot{x}(t) = \begin{pmatrix} \dot{q}(t) \\ \ddot{q}(t) \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{D}{m} \end{pmatrix} x(t) + \begin{pmatrix} 0 \\ \frac{1}{m} \end{pmatrix} u(t)$$

$$M\ddot{q} + D\dot{q} + kq = 0$$

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{pmatrix} = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \end{pmatrix} u$$

$$U = \begin{pmatrix} 1/s \\ 1/s \\ 4s/s \\ 1/s \end{pmatrix}$$

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{pmatrix} = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \end{pmatrix} u$$

$$F = ma \Rightarrow a = \frac{F}{m}$$

$$\begin{pmatrix} \dot{q}(t) \\ \ddot{q}(t) \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{D}{m} \end{pmatrix} \begin{pmatrix} q(t) \\ \dot{q}(t) \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{1}{m} \end{pmatrix} u(t)$$

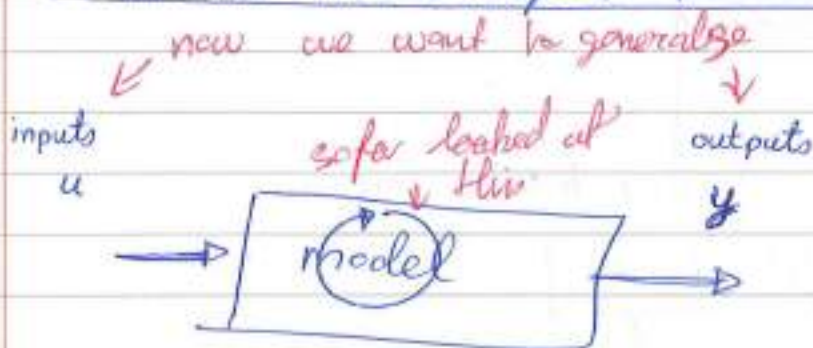
only output: $-y(t) = (1 \ 0) x(t) + 0 u(t)$

$$\begin{pmatrix} q(t) \\ \dot{q}(t) \end{pmatrix}$$

input

Mathematical Modelling. Lecture 3.

Continuous-time transfer, Laplace transform & impulse response



Ex. of second order linear diff. equation

$$* \Rightarrow y''(t) + 3y'(t) - y(t) = 4u''(t) + u'(t) + 3u$$

Laplace Transformation.

lower case for time func.

upper case for transformed.

we consider $f(t)$ which have $f(t) = 0$ for $t < 0$, thus we start at 0.

can generalise to two-sided $\mathcal{L}$ with $(-\infty)$.

s complex

$s = i\omega$ ($\omega \in \mathbb{R}$)

s relates to frequencies (more complex def. will follow).

linear transformation

$$f(t) \xrightarrow{\mathcal{L}} F(s) := \int_0^{\infty} f(t) e^{-st} dt$$

$C_1 f_1(t) + C_2 f_2(t) \xrightarrow{\mathcal{L}} C_1 F_1(s) + C_2 F_2(s)$

$$f(t) = e^{2t}$$

we consider

$$[F(s)] = \int_0^{\infty} e^{2t} \cdot e^{-st} dt = \int_0^{\infty} e^{(2-s)t} dt = \frac{1}{2-s} e^{(2-s)t} \Big|_0^{\infty}$$

$$= 0 - \frac{1}{2-s} \times e^{(2-s)0} = 0 - \frac{1}{2-s} = \boxed{\frac{1}{s-2}}$$

$$u(t) \xrightarrow{\mathcal{L}} U(s)$$

$$y(t) \xrightarrow{\mathcal{L}} Y(s)$$

$\mathcal{L}$
(Laplace transformation).

$$f(t) \xrightarrow{\mathcal{L}} F(s)$$

$$f'(t) \xrightarrow{\mathcal{L}} sF(s) - f(0) = sF(s)$$

we take at condition where initially zero

$$f''(t) \xrightarrow{\mathcal{L}} s^2 F(s)$$

$$* s^2 Y(s) + 3s Y(s) - Y(s) = 4s^2 U(s) + s U(s) + 3U(s)$$

$$(s^2 + 3s - 1) Y(s) = (4s^2 + s + 3) U(s)$$

$$Y(s) = \frac{4s^2 + s + 3}{s^2 + 3s - 1} \cdot U(s)$$

transform output depends on $\uparrow$ transform of input multiplied by some value/constant.

$H(s)$ transfer func.

$$Y(s) = H(s) \cdot U(s)$$

$\uparrow$ output $\uparrow$ system $\uparrow$ input.

Ex of 'L'

$$f(t) = x'(t) = 3x(t) - 5e^{-2t} + 1 \quad x(0) = 6$$

$sF(s) - f(0) \rightarrow cF(s)$ $\downarrow$ intable $\downarrow$ intable

$$sX(s) - 6 = 3X(s) - 5 \cdot \frac{1}{s+2} + \frac{1}{s}$$

$$(s-3)X(s) = -\frac{5}{s+2} + \frac{1}{s} + 6$$

$$\frac{e^{at}}{s-a} = \frac{1}{s-a}$$

$$X(s) = \frac{-5}{(s+2)(s-3)} + \frac{1}{s(s-3)} + \frac{6}{(s-3)}$$

$\Downarrow \mathcal{L}^{-1}$

$$\frac{-5}{(s+2)(s-3)} = \frac{1}{(s+2)} - \frac{15}{(s-3)}$$

$$\frac{1}{s(s-3)} = -\frac{1/3}{s} + \frac{1/3}{s-3}$$

use comp. these in the $\frac{1}{s-a}$ form

$$e^{-2t} - e^{3t} - \frac{1}{3} + \frac{1}{3}e^{3t}$$

$$6e^{3t}$$

$$x(t) = e^{-2t} + \frac{16}{3}e^{3t} - \frac{1}{3}$$

check $x(0) = 1 + \frac{16}{3} - \frac{1}{3} = 6 //$

Verifg. $x'(t) = -2e^{-2t} + 3(x(0) - \frac{2}{3})e^{3t} = -2e^{-2t} + (3x(0) - 2)e^{3t}$

rhs = $s(x(t)) - 5e^{-2t} + 1 = 3e^{-2t} + (3x(0) - 2)e^{3t} - 1 - 5e^{-2t} + 1$

$= -2e^{-2t} + (3x(0) - 2)e^{3t}$

$\swarrow$ equal

no a_0 or $a_0 = 1$ by convention.

$$y^{(n)}(t) + a_1 y^{(n-1)}(t) + \dots + a_n y(t) =$$

$$= b_0 u^{(n)}(t) + b_1 u^{(n-1)}(t) + \dots + b_n u(t)$$

n^{th} order diff. equ.

$$H(s) = \frac{b_0 s^n + b_1 s^{n-1} + \dots + b_n}{s^n + a_1 s^{n-1} + \dots + a_n}$$

linear transformation of input.

$$Y(s) = H(s) U(s)$$

if $U(s) = 1$ then $Y(s) = H(s)$
 $\uparrow$
 $u(t) = ?$
 $y(t) = h(t)$

- solving high order linear D.E. may be difficult but w/ 'L' just multiply by $H(s)$

- the output obtained from input by the "action" of the system, can use to tell which outputs affect which inputs, and what from the dynamics of the system.

impulse function:



when this func gets higher the duration gets relatively shorter and at ∞ it ends up as $\delta(t)$.

Area under the func. is 1 all the time. (can have multiples of $\delta(t)$ "delta func".)

$$\Delta(s) \int_0^{\infty} \delta(t) e^{-st} dt = 1$$

$$\int_0^{\infty} \delta(t) f(t) dt = f(0) \text{ and } e^0 = 1$$

So back to

$$U(s) = 1$$



$$u(t) = \delta(t)$$

impulse
(input)

$$Y(s) = H(s)$$

$$y(t) = h(t)$$

impulse response
(output)

Laplace transform of impulse response = transfer func.

$$h(t) \xrightarrow{\mathcal{L}} H(s)$$

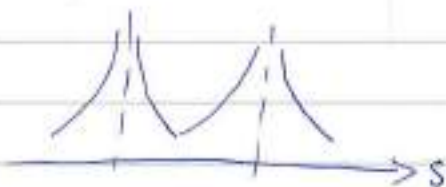
going from $H(s)$ (rational, degree n)

to a sum of easier rational functions all of degree ≤ 1 .

partial fraction expansion (PFE)

$$H(s) = \frac{2s + 3}{s^2 + 4s + 3} = \frac{C_1}{s+1} + \frac{C_2}{s+3}$$

zeros of the denominator = poles of $H(s)$



$$s^2 + 4s + 3 = (s+1)(s+3)$$

$$\frac{C_1(s+3) + C_2(s+1)}{(s+1)(s+3)} = \frac{(C_1 + C_2)s + 3C_1 + C_2}{(s+1)(s+3)}$$

Ex.

$$H(s) = \frac{26}{s^3 + s^2 - 7s - 15}$$

$$h(t) = ?$$

step 1: poles of $H(s)$: $s^3 + s^2 - 7s - 15 = 0$

$$3^3 + 3^2 - 7 \cdot 3 - 15 = 0.$$

Factor $s-3$.

$$s^3 + s^2 - 7s - 15 = (s-3)(s^2 + 4s + 5)$$

$$H(s) = \frac{26}{(s-3)(s+2-j)(s+2+j)}$$

$$H(s) = \frac{26}{(s-3)(s+2-i)(s+2+i)}$$

$$= \underset{\substack{\parallel \\ 0}}{A_0} + \frac{A_1}{s-3} + \frac{A_2}{s+2-i} + \frac{A_3}{s+2+i}$$

$$H(s)(s-3) = \frac{26}{s^2+4s+5} = A_1 + \frac{A_2(s-3)}{(s+2-i)} + \frac{A_3(s-3)}{(s+2+i)}$$

plug in $s=3$

$$\frac{26}{9+12+5} = A_1 = 1$$

Ex. worked out in notes. $A_2 = \frac{-1+5i}{2}$ $A_3 = \frac{-1-5i}{2}$

$$A_2 = \frac{26}{(s-3)(s+2+i)} \Big|_{s=-2-i} = \frac{26}{(-5+i) \cdot 2i} = \frac{26}{-2-10i} = \frac{-1+5i}{2}, \quad A_3 = A_2^* = \frac{-1-5i}{2}$$

Partial Fraction Expansion Example.

$$H(s) = \frac{2s^3 - 3s^2 + 7s + 4}{s^3 + 6s^2 + 11s + 6}, \text{ find } h(t)$$

Step 1: find the poles of $H(s)$, need to solve $s^3 + 6s^2 + 11s + 6 = 0$, gives $-1, -2, -3$.
writing $s^3 + 6s^2 + 11s + 6 = (s+1)(s+2)(s+3)$ we get.

$$\frac{2s^3 - 3s^2 + 7s + 4}{(s+1)(s+2)(s+3)} = A_0 + \frac{A_1}{(s+1)} + \frac{A_2}{(s+2)} + \frac{A_3}{(s+3)}$$

$$\frac{2s^3 - 3s^2 + 7s + 4}{(s+2)(s+3)} = A_0(s+1) + \frac{A_2(s+1)}{(s+2)} + \frac{A_3(s+1)}{(s+3)}$$

sub $s=-1$

$$\frac{-2-3-7+4}{2} = A_1 \Rightarrow A_1 = -4$$

sub $s=-2$

$$\frac{16-12-14+4}{-1} = A_2 \Rightarrow A_2 = 38$$

sub $s=-3$

$$\frac{-54-27-21+4}{-2} = A_3 \Rightarrow A_3 = -49$$

$$\text{As } s \rightarrow \infty \rightarrow 2. \quad A_0 = 2.$$

$$h(t) = 2\delta(t) - 4e^{-t} + 38e^{-2t} - 49e^{-3t}$$

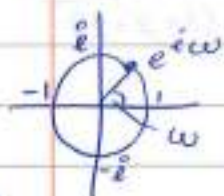
As $s \rightarrow \infty$, equation tends to 2.

$$H(s) = \frac{1}{s-3} + \frac{-1+5i}{2} \cdot \frac{1}{s+2-i} + \frac{-1-5i}{2} \cdot \frac{1}{s+2+i}$$

$$\mathcal{L}^{-1} \downarrow$$

$$h(t) = e^{3t} + \frac{-1+5i}{2} \cdot e^{(-2+i)t} + \frac{-1-5i}{2} \cdot e^{(-2-i)t}$$

$$e^{(-2+i)t} = e^{-2t} \cdot e^{it} = e^{-2t} (\cos(t) + i \sin(t))$$



$$e^{(-2-i)t} = e^{-2t} \cdot e^{-it} = e^{-2t} (\cos(t) - i \sin(t))$$

Ch 4. Ex 4.
HW.

$$\begin{aligned} h(t) &= e^{3t} - \frac{1+5i}{2} (e^{-2t} (\cos(t) + i \sin(t))) - \frac{1-5i}{2} (e^{-2t} (\cos(t) - i \sin(t))) \\ &= \frac{e^{3t}}{2} (-1+5i (e^{-2t} (\cos(t) + i \sin(t))) - 1-5i (\cos(t) + i \sin(t))) \\ &= \frac{e^{3t}}{2} ((e^{-2t} + 5i e^{-2t}) (\cos(t) + i \sin(t)) - (e^{-2t} - 5i e^{-2t}) (\cos(t) - i \sin(t))) \\ &= \frac{e^{3t}}{2} (\cos(t) + i \sin(t)) \end{aligned}$$

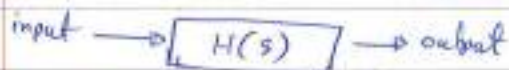
Mathematical Modelling Lecture 4

Continuous-time transfer functions with repeated roots and the z-domain.

Ex. Nr. 7.

$$H(s) = - \frac{s^2 - 12s + 11}{s^3 + s + 10}$$

impulse



$$Y(s) = H(s) U(s)$$

$$u(t) = \delta(t) \quad U(s) = \Delta(s) = 1$$

impulse

impulse response.

$h(t)$

$$H(s) = - \frac{s^2 - 12s + 11}{s^3 + s + 10}$$

$$= - \frac{s^2 - 12s + 11}{(s+2)(s-(1+2i))(s-(1-2i))}$$

$$= A_0 + \left[\frac{A_1}{(s+2)} + \frac{A_2}{(s-(1+2i))} + \frac{A_3}{(s-(1-2i))} \right]$$

$$s^3 + s + 10 = 0$$

$$s = -2 \quad \text{solution}$$

$s+2$ is a factor

$$s^3 + s + 10 = (s+2)(s^2 - 2s + 5)$$

$$s^2 - 2s + 5 = 0 \quad s = 1 \pm 2i$$

$$\frac{-b \pm \sqrt{b^2 - 4ac}}{2a} = \frac{+2 \pm \sqrt{4 - 20}}{2} = \frac{2 \pm \sqrt{-16}}{2} = \frac{2 \pm 4\sqrt{-1}}{2} = 1 \pm 2i$$

$$s - (1+2i) = 0$$

$$s - (1-2i) = 0$$

$$A_1 = H(s)(s+2) = A_1 + \frac{A_2(s+2)}{s-(1+2i)} + \frac{A_3(s+2)}{s-(1-2i)} \Big|_{s=-2}$$

$$A_1 = - \frac{s^2 + 12s - 11}{s^2 - 2s + 5} \Big|_{s=-2} = \frac{-4 - 24 - 11}{4 + 4 + 5} = \frac{-39}{13} = -3 //$$

$$A_2 = H(s)(s-(1+2i)) \Big|_{s=1+2i}$$

$$= - \frac{s^2 + 12s - 11}{(s+2)(s-(1-2i))} \Big|_{s=1+2i} = \frac{(1+2i)^2 + 12(1+2i) - 11}{(1+2i+2)(1+2i-1+2i)}$$

$$A_2 = 1 - i //$$

$$= \frac{(1+4i-4) + 12+24i - 11}{-8+12i}$$

$$A_3 = 1 + i //$$

$$= \frac{4+20i}{-8+12i} = \frac{1+5i}{-2+3i} \cdot \frac{-2-3i}{-2-3i}$$

$$= \frac{-2-10i-3i+15}{4+9} = \frac{13-13i}{13} = 1-i //$$

$$H(s) = \frac{-3}{s+2} + \frac{1-i}{s-(1+2i)} + \frac{1+i}{s-(1-2i)}$$

$$h(t) = -3e^{-2t} + (1-i) \cdot e^{(1+2i)t} + (1+i) \cdot e^{(1-2i)t}$$

$$e^{i\phi} = \cos(\phi) + i\sin(\phi)$$

$$(1-i)e^t e^{2it}$$

$$(1-i)e^t (\cos(2t) + i\sin(2t))$$

$$e^t (\cos(2t) - i\cos(2t) + i\sin(2t) + \sin(2t))$$

$$\Rightarrow e^t (\cos(2t) + i\cos(2t) - i\sin(2t) + \sin(2t)) +$$

$$\Rightarrow 2e^t (\cos(2t) + \sin(2t))$$

$$h(t) = -3e^{-2t} + 2e^t (\cos(2t) + \sin(2t)) //$$

$$H(s) = \frac{1}{(s+1)(s+2)^2}$$

$$H(s) = \frac{A_1}{(s+1)} + \frac{A_2}{(s+2)} + \frac{A_3}{(s+2)^2}$$

$$h(t) = A_1 e^{-t} + A_2 e^{-2t} + A_3 t e^{-2t}$$

$$t^k e^{at} \rightarrow \frac{k!}{(s-a)^{k+1}}$$

damped polynomial in sheet

Suppose there is a pole at $\boxed{s=q}$ with multiplicity m .

$$H(s) = \frac{\dots}{(s-q)^m(\dots)}$$

$$\text{include: } \frac{B_1}{s-q} + \frac{B_2}{(s-q)^2} + \frac{B_3}{(s-q)^3} + \dots + \frac{B_m}{(s-q)^m} + \text{other terms.}$$

$$H(s) \cdot (s-q)^m$$

$$B_1(s-q)^{m-1} + B_2(s-q)^{m-2} + \dots + B_{m-1}(s-q) + B_m$$

$$\text{set } s=q \Rightarrow B_m$$

other term = $(s-q)^m$

$$H(s) \cdot (s-q)^m \Big|_{s=q} = B_m$$

diff. $H(s)(s-q)^m$:

$$(s-q)^1 = 1$$

$$(m-1)B_1(s-q)^{m-2} + (m-2)B_2(s-q)^{m-3} + \dots + B_{m-1} \cdot 1 + 0 + (s-q)^m \text{ other terms}$$

$$|_{s=q} \Rightarrow B_{m-1}$$

$$\frac{d^k}{ds^k} H(s)(s-q)^m \Big|_{s=q} = k! B_{m-k}$$

BIBO stability

bounded input bounded output.

$$u(t) \rightarrow \boxed{H(s)} \rightarrow y(t)$$

$$Y(s) = H(s) U(s)$$

$$y(t) = \int_0^t h(\tau) u(t-\tau) d\tau$$

convolution integral
between $u(t)$ and $h(t)$

$$= \int_0^t u(\tau) h(t-\tau) d\tau$$

Suppose $\int_0^\infty |h(t)| dt = M < \infty$

$$|y(t)| = \left| \int_0^t h(\tau) u(t-\tau) d\tau \right| \leq \int_0^t |h(\tau)| |u(t-\tau)| d\tau$$

bounded by B

$$\leq \int_0^t |h(\tau)| dt \cdot B$$

so $\int_0^t |h(\tau)| dt \leq M$

$$\leq M \cdot B$$

$$H(s) = \frac{1}{s+5} \rightarrow h(t) = e^{-5t} + e^{-2t}$$

$$\frac{1}{s+2} \quad \int_0^\infty |h(t)| dt < \infty$$

$$\int_0^\infty e^{-5t} dt = -\frac{1}{5} e^{-5t} \Big|_0^\infty = \left[0 + \frac{1}{5} e^0 \right] = \frac{1}{5}$$

BIBO stable.

$$\int_0^\infty e^{-2t} dt = -\frac{1}{2} e^{-2t} \Big|_0^\infty = \left[0 + \frac{1}{2} \right] = \frac{1}{2}$$

BIBO stable

$$\frac{1}{s-5} \rightarrow e^{5t} \xrightarrow{t \rightarrow \infty} \infty$$

not BIBO stable.

$$3e^{(-2+i)t} + 3e^{(-2-i)t}$$

$$3e^{-2t} \cdot e^{it} + 3e^{-2t} \cdot e^{-it}$$

absolute values of these, as they are purely imaginary, will be 1.

You will always converge if $e^{-ive \text{ real}}$ or $e^{-ive \text{ real part} + i \text{ whatever}}$

this is the only part that matters.

BIBO stability for our class of systems.

It requires that all poles have a -ive real part.

Asymptotic stability.

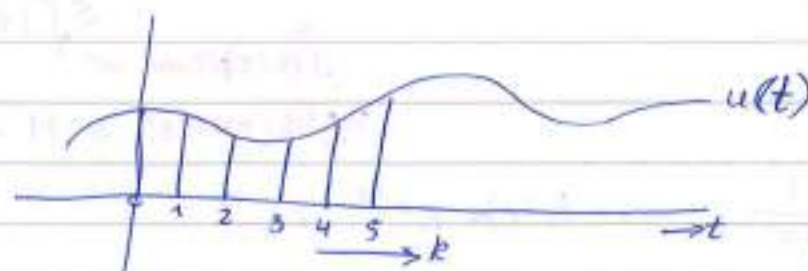
if the output goes to zero if we apply a zero input (start from any arbitrary initial position)

if $h(t) \rightarrow 0$ for $t \rightarrow \infty$: asymptotic stability
 $\rightarrow 0$ not so

CONTINUOUS TIME

continuous-time: $u(t)$ $y(t)$, $x(t)$
 $t \in \mathbb{R}$ $[0, \infty)$

discrete-time: time(index) k
 $k \in \mathbb{Z}$ $k = 0, 1, 2, 3, \dots$



$\{u[0], u[1], u[2], \dots\}$

Δt : sampling time

= interval between consecutive samples

$$t = k \cdot \Delta t \quad u[2] = u(2 \cdot \Delta t)$$

difference equations instead of differential equations.

$$x'(t) = a x(t) \quad x(0) = x_0$$

$$x(t) = e^{at} x_0$$

$$\Delta t = 1 \quad x[k] = x(h) = e^{ah} x_0$$

$$e^0 x_0, e^a x_0, e^{2a} x_0, e^{3a} x_0, \dots$$

$$x_0, e^a x_0, (e^a)^2 x_0, (e^a)^3 x_0, \dots$$

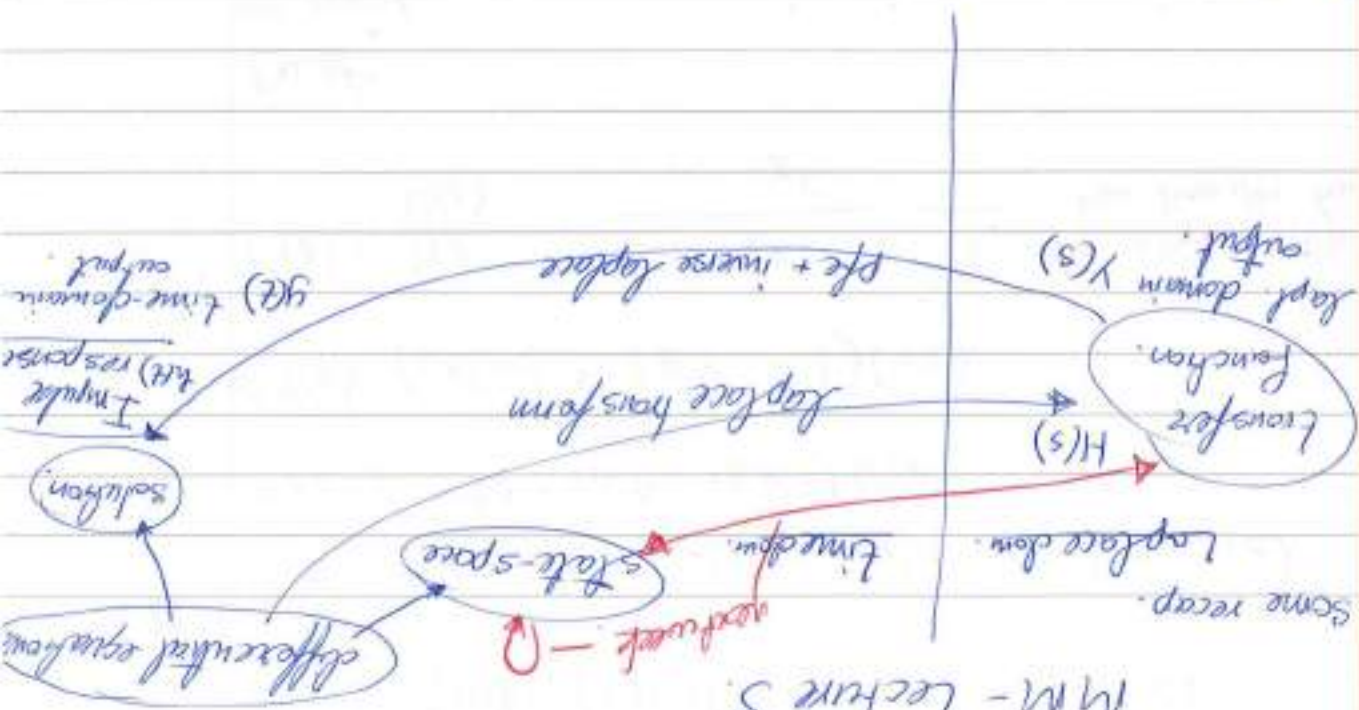
$$x[0], x[1], x[2], x[3]$$

$$x[k+1] = e^a \cdot x[k] \quad x[0] = x_0$$

difference equation



MM - Lecture 5



Today.

Discrete-Time (of all the stuff above)

sampling interval $T = 1 \text{ day} = 24 \cdot 60 \cdot 60 \text{ s} = 86,400 \text{ s}$
 sampling frequency $f_s = \frac{1}{T} = 0.00001157407 \text{ Hz}$

1 day average can be written as a difference equation

$$y[k] = \frac{1}{T} u[k] + \frac{1}{T} u[k-1] + \frac{1}{T} u[k-2] + \dots + \frac{1}{T} u[k-6]$$

k is time index, corresponding to time $t_0 + kT$
 $[]$ to indicate discrete.

For z -transform

difference equation — derivatives — Laplace.
 difference equation — time delay — z -transform

z -transform of sequence $\{f[k]\}$

$$F(z) = \sum_{k=0}^{\infty} f[k] z^{-k}$$

$k < 0$

to note similarities between discrete & $F(s) = \int_0^{\infty} f(t) e^{st} dt$
 continuous.

Ex. $y[k] = \frac{1}{2}u[k] + \frac{1}{2}u[k-1] + \frac{1}{2}u[k-2] + \dots + \frac{1}{2}u[k-3]$

$Y(z) = \frac{1}{2}U(z) + \frac{1}{2}z^{-1}U(z) + \frac{1}{2}z^{-2}U(z) + \dots + \frac{1}{2}z^{-3}U(z)$

$Y(z) = \left(\frac{1}{2} + \frac{1}{2}z^{-1} + \frac{1}{2}z^{-2} + \dots + \frac{1}{2}z^{-3}\right)U(z)$

$H(z) = \frac{Y(z)}{U(z)} = \frac{1}{2}z^0 + \frac{1}{2}z^{-1} + \frac{1}{2}z^{-2} + \dots + \frac{1}{2}z^{-3}$

$H(z) = \frac{Y(z)}{U(z)} = \frac{1}{2}z^0 + \frac{1}{2}z^{-1} + \frac{1}{2}z^{-2} + \dots + \frac{1}{2}z^{-3}$
This is your discrete time transfer function.

Ex. *non-causal.*

$y[k] = \frac{1}{2}u[k] + \frac{1}{2}u[k+1] + \frac{1}{2}u[k+2] + \dots + \frac{1}{2}u[k+3]$



$Y(z) = \left(\frac{1}{2}z^3 + \frac{1}{2}z^2 + \frac{1}{2}z^1 + \frac{1}{2}z^0 + \frac{1}{2}z^{-1} + \frac{1}{2}z^{-2} + \frac{1}{2}z^{-3}\right)U(z)$

but output depends on values yet to come.

$H(z) = \frac{Y(z)}{U(z)} = \frac{1}{2}z^3 + \frac{1}{2}z^2 + \frac{1}{2}z^1 + \frac{1}{2}z^0 + \frac{1}{2}z^{-1} + \frac{1}{2}z^{-2} + \frac{1}{2}z^{-3}$

$\frac{z^3}{\left(\frac{1}{2}z^6 + \frac{1}{2}z^5 + \frac{1}{2}z^4 + \dots + \frac{1}{2}z^1 + \frac{1}{2}z^0\right)}$

so improper

causality relates directly

to properness of the system.

Abk. 4.3. Properties of z-transform

Back to causal.

$$H(z) = \frac{Y(z)}{X(z)} = \frac{\frac{1}{2}z^6 + \frac{1}{2}z^5 + \dots + \frac{1}{2}}{z^6}$$

proper moving-average filter (all poles at 0).

Linearity

$$\alpha_1 f_1[k] + \alpha_2 f_2[k] \leftrightarrow \alpha_1 F_1(z) + \alpha_2 F_2(z)$$

Time-delay

$$g[k] = f[k-1] \quad G(z) = z^{-1}F(z)$$

Time-advance

$$g[k] = f[k+1] \quad G(z) = zF(z)$$

Convolution in time domain $\leftrightarrow$ Multiplication in z domain

$$f_1[k] \otimes f_2[k] \leftrightarrow F_1(z)F_2(z)$$

convolution in time domain

$$= \sum_{i=0}^k f_1[i]f_2[k-i]$$

$$= \sum_{i=0}^k f_1[k-i]f_2[i]$$

Linear Difference Equation

$$y[k] + a_1 y[k-1] + \dots + a_n y[k-n] = b_0 u[k] + b_1 u[k-1] + \dots + b_n u[k-n]$$

$$\xrightarrow{Z} (1 + a_1 z^{-1} + \dots + a_n z^{-n}) Y(z) = (b_0 + b_1 z^{-1} + \dots + b_n z^{-n}) U(z)$$

$$(z^n + a_1 z^{n-1} + \dots + a_n) Y(z) = (b_0 z^n + b_1 z^{n-1} + \dots + b_n) U(z)$$

transfer function

$$H(z) = \frac{Y(z)}{U(z)} = \frac{(z^n + a_1 z^{n-1} + \dots + a_n)}{(b_0 z^n + b_1 z^{n-1} + \dots + b_n)}$$

$$Y(z) = H(z)U(z)$$

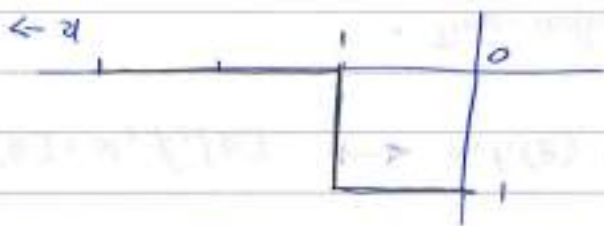
Z-domain output

$$Y(z) = H(z)U(z)$$

like w/ CT systems we can obtain $Y(z) = H(z)U(z)$ by choosing $U(z) = 1$.

what $u[k]$ has z-transform $U(z) = 1$?

DT impulse (Kronecker delta) $\delta[k] = \begin{cases} 1 & k=0 \\ 0 & \text{else} \end{cases}$



Break

Let a system be governed by

$$y[k] - 2y[k-1] - 3y[k-2] = u[k-2]$$

$$(1 - 2z^{-1} - 3z^{-2})Y(z) = z^{-2}U(z)$$

$$H(z) = \frac{Y(z)}{U(z)} = \frac{1 - 2z^{-1} - 3z^{-2}}{z^{-2}} = \frac{z^2 - 2z - 3}{1}$$

What is the impulse response?

output corresponding to input $u[k] = \delta[k]$

$$Y(z) = H(z)U(z) = H(z) = \frac{z^2 - 2z - 3}{1}$$

Do PFE on $\frac{z}{Y(z)}$ for D.T.

to then expand, ~~convert~~ then return back to normal, then hang on

to $h[k]$

Ex:

$$H(z) = \frac{z^3 - 2z^2 - 3z}{1} = \frac{z}{A_0} + \frac{z+1}{A_1} + \frac{z-3}{A_2}$$

extra pole at 0.0

$$A_0 = H(0) = -\frac{3}{1}$$

$$A_1 = \frac{z}{H(z)(z+1)} \Big|_{z=-1} = \frac{z(2/1)(z-3)}{(z+1)^1} \Big|_{z=-1} = \frac{1}{4}$$

$$A_2 = \frac{z}{H(z)(z-3)} \Big|_{z=3} = \frac{z(2/1)(2/3)}{(z-3)^1} \Big|_{z=3} = \frac{1}{12}$$

$$H(z) = -\frac{3}{1} + \frac{1}{4} \frac{z}{(z+1)} + \frac{1}{12} \frac{z}{(z-3)}$$

$$H(z) = -\frac{1}{3} + \frac{1}{4} \frac{(z+1)}{z} + \frac{1}{12} \frac{(z-3)}{z}$$

$$h[k] = -\frac{1}{3} \delta[k] + \frac{1}{4} (-1)^k + \frac{1}{12} (3)^k$$

↑
from long

→ Generic (avoiding repeated poles)

$$H(z) = \frac{b(z)}{a(z)}$$

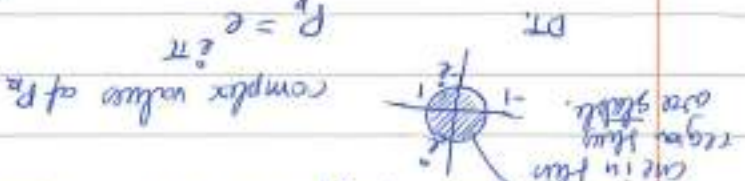
$$\frac{H(z)}{z} = \frac{A_0}{z} + \frac{A_1}{z-p_1} + \frac{A_2}{z-p_2} + \dots + \frac{A_n}{z-p_n}$$

$$H(z) = A_0 + A_1 \frac{z-p_1}{z} + A_2 \frac{z-p_2}{z} + \dots + A_n \frac{z-p_n}{z}$$

$$h[k] = A_0 \delta[k] + A_1 (p_1)^k + A_2 (p_2)^k + \dots + A_n (p_n)^k$$

when stable BIBO $\|h[k]\| < \infty$

as long as pole $|p_k| < 1 \forall k$ stable



DT.
 $p_k = e^{j\pi}$
 $(p_k)^\delta = e^{j\pi\delta}$
 most cases you'll be within the unit circle not on it.

Mathematical Modelling Lecture 6.

So far,

• high order differential equations.

$$u, u', u'', \dots, u^{(n)} \quad a_1, \dots, a_n, b_0, b_1, \dots, b_n$$
$$y, y', y'', \dots, y^{(n)}$$

• transfer function.

$$\frac{b_0 s^n + b_1 s^{n-1} + \dots + b_n}{s^n + a_1 s^{n-1} + \dots + a_n}$$

• impulse response

$$\begin{array}{c} \uparrow \mathcal{L} \\ h(t) \end{array}$$

• state-space systems

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases}$$
$$x(t) \in \mathbb{R}^n$$

$$f(t) \rightarrow \int_0^{\infty} f(t) e^{-st} dt = F(s)$$

$$af(t) \xrightarrow{\mathcal{L}} aF(s)$$

$$\begin{pmatrix} f_1(t) \\ \vdots \\ f_n(t) \end{pmatrix} \rightarrow \begin{pmatrix} \int_0^{\infty} f_1(t) e^{-st} dt \\ \vdots \\ \int_0^{\infty} f_n(t) e^{-st} dt \end{pmatrix} = F(s)$$

also a vector function.

$$Af(t) \xrightarrow{\mathcal{L}} AF(s)$$

Now apply Laplace to the ss system.

$$X(s) = (sI - A)^{-1} B U(s)$$

$$Y(s) = [C(sI - A)^{-1} B + D] U(s)$$

$$Y(s) = H(s) U(s)$$

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

↓

$$\begin{cases} sX(s) = AX(s) + BU(s) \\ Y(s) = CX(s) + DU(s) \end{cases}$$

$$\Rightarrow sX(s) - AX(s) = BU(s)$$

$$\Rightarrow (sI - A)X(s) = BU(s)$$

$$X(s) = (sI - A)^{-1} BU(s)$$

$$Y(s) = CX(s) + DU(s)$$

$$= C(sI - A)^{-1} BU(s) + DU(s)$$

$$Y(s) = [C(sI - A)^{-1} B + D] U(s)$$

$$H(s) = C(sI - A)^{-1}B + D$$

transfer func.

Ex. $A = \begin{pmatrix} 2 & -1 \\ 4 & 5 \end{pmatrix}$ $sI - A = \begin{pmatrix} s & 0 \\ 0 & s \end{pmatrix} - \begin{pmatrix} 2 & -1 \\ 4 & 5 \end{pmatrix}$

$$\begin{pmatrix} a & b \\ c & d \end{pmatrix} = \frac{1}{ad - bc} \begin{pmatrix} d & -b \\ -c & a \end{pmatrix} \quad \downarrow \text{inversion.}$$

$$(sI - A)^{-1} = \frac{\begin{pmatrix} s-5 & -1 \\ 4 & s-2 \end{pmatrix}}{(s-2)(s-5) + 4}$$

// degree of numerator ≤ 2
// " " denominator = 2

row vec $C = (\dots \dots \dots)$ col vec $B = \begin{pmatrix} \vdots \\ \vdots \\ \vdots \\ \vdots \end{pmatrix}$

denominator of transfer function.

$$= \det(sI - A)$$

characteristic polynomial of A .

$$(sI - A)^{-1} = \frac{\text{adj}(sI - A)}{\det(sI - A)}$$

zeros of the denominator
=
eigen values of A
=
poles of $H(s)$

eigenvalues of A determine the stability of a state-space system.

$$H(s) = \frac{b_0 s^n + \dots + b_n}{s^n + a_1 s^{n-1} + \dots + a_n}$$

$2n+1$ parameters.

statespace (A, B, C, D)

$$H(s) = C(sI - A)^{-1}B + D$$

$$\begin{pmatrix} A \end{pmatrix}_{n \times n} \quad \begin{pmatrix} B \end{pmatrix}_{n \times 1}$$

$$\begin{pmatrix} C \end{pmatrix}_{1 \times n} \quad \begin{pmatrix} D \end{pmatrix}_{1 \times 1}$$

extra parameters lots of freedom.

$n^2 + 2n + 1$
parameters

system $\dot{x}(t) = Ax(t) + Bu(t)$
 $y(t) = Cx(t) + Du(t)$

new state vector: $\tilde{x}(t) = T x(t)$

T : $n \times n$ matrix
invertible.

$$\tilde{x}'(t) = T x'(t)$$

$$\tilde{x}'(t) = T x'(t) = T A x(t) + T B u(t)$$

$$x(t) = T^{-1} \tilde{x}(t)$$

$$\boxed{\begin{aligned} \tilde{x}'(t) &= (T A T^{-1}) \tilde{x}(t) + (T B) u(t) \\ y(t) &= (C T^{-1}) \tilde{x}(t) + D u(t) \end{aligned}}$$

new linear state space with
changed coordinates of
 $\tilde{x}(t)$ instead of $x(t)$

so the transfer func. must be ~~unchanged~~
unchanged.

$$C(sI - A)^{-1} B + D = C \underbrace{T^{-1} (sI - T A T^{-1})^{-1} T}_{T = (T^{-1})^{-1}} B + D$$

$$C (T^{-1} (sI - T A T^{-1}) T) B + D$$

$$\underbrace{s T^{-1} I T - A}_{sI - A}$$

$$\begin{aligned} (PQR)^{-1} &= R^{-1} Q^{-1} P^{-1} \\ &= \left(\begin{matrix} T^{-1} \\ sI - T A T^{-1} \\ T \end{matrix} \right)^{-1} \\ &= T (sI - T A T^{-1})^{-1} T^{-1} \end{aligned}$$

so here we show even if we do a
linear transformation on our state
the transfer function is still the
same in general.

$$\begin{aligned} (PQR)' &= (T^{-1} * (sI - T A T^{-1}) * T)^{-1} \\ &= (T^{-1} sI T - T^{-1} T A T^{-1} T)^{-1} \\ &= (sI - A)^{-1} \end{aligned}$$

from a transfer function to a state-space system.
(general given transfer func.)

$$H(s) = \frac{b_0 s^n + \dots + b_n}{s^n + a_1 s^{n-1} + \dots + a_n}$$

$$\rightarrow (A, B, C, D)$$

s.t.

column of n-1's, add I

$$A = \begin{pmatrix} -a_1 & 1 & 0 & \dots & 0 \\ -a_2 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -a_{n-1} & 0 & \dots & 0 & 1 \\ -a_n & 0 & \dots & 0 & 0 \end{pmatrix}$$

add row of zeros

$$C(sI - A)^{-1} B + D = H(s)$$

$$B = \begin{pmatrix} b_1 - b_0 a_1 \\ b_2 - b_0 a_2 \\ \vdots \\ b_n - b_0 a_n \end{pmatrix}$$

subtract $b_0 a_i$

$$C = (1 \mid 0 \dots \dots 0)$$

$$D = b_0$$

col. of b's
just always b_0 .

→ observable canonical form.

Ex. to show it works.

$$c(sI - A)^{-1}B + D.$$

$$(1 \ 0 \ \dots \ 0) \begin{pmatrix} s+a_1 & -1 & & 0 \\ a_2 & s & & 0 \\ & & \ddots & \\ a_n & 0 & & s \end{pmatrix}^{-1} = (w_1 \ w_2 \ \dots \ w_n)$$

-1 is on off diagonal.

$$(1 \ 0 \ \dots \ 0) = (w_1 \ w_2 \ \dots \ w_n) \begin{pmatrix} s+a_1 & -1 & & 0 \\ a_2 & s & & 0 \\ & & \ddots & \\ a_n & 0 & & s \end{pmatrix}$$

-1 on off diagonal.

$$(s^n + a_1 s^{n-1} + a_2 s^{n-2} + \dots + a_{n-1} s + a_n) \cdot (1 \ 0 \ \dots \ 0).$$

$$(w_1 \ \dots \ w_n) = \frac{(s^{n-1}, s^{n-2}, \dots, s, 1)}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$

now you multiply the above

by B to finally produce the $c(sI - A)^{-1}B$. The b_i -bars cancel out with the a values to produce the $c(sI - A)^{-1}B$ as we've defined before.

$$H(s) = \frac{b_0 s^n + b_1 s^{n-1} + \dots + b_n}{s^n + a_1 s^{n-1} + \dots + a_n}$$

→ controllable canonical form.

$$A = \begin{pmatrix} -a_1 & \dots & -a_n \\ 1 & & 0 \\ & \ddots & \\ 0 & & 1 \end{pmatrix} \quad B = \begin{pmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{pmatrix}$$

$$C = (b_1 - b_0 a_1, \dots, b_n - b_0 a_n) \quad D = b_0$$

$$H(s) = c(sI - A)^{-1}B + D$$

$$(SI-A)^{-1} = ? = \frac{\det(SI-A)}{\dots}$$

$$\left(\begin{array}{ccc|ccc} 5 & -6 & 7 & 3 & 1 & 0 & 0 \\ -1 & 5 & 11 & 0 & 1 & 0 & 0 \\ 0 & 2 & 8 & 3 & 0 & 0 & 1 \end{array} \right)$$

5 (but this is a pain in the ass)

$$(SI-A)^{-1} = ? = \frac{\det(SI-A)}{\det(SI-A)}$$

$$\det(SI-A) = a(a) = a^n + a_1 a^{n-1} + \dots + a_{n-1} a + a_n$$

$$S_1 = I_n \rightarrow AS_1 = A = S_1 A \quad a_1 = \text{trace}(A)$$

trace is the sum of entries on main diagonal.

$$S_2 = AS_1 + a_1 I_n \rightarrow AS_2 \quad a_2 = -\text{trace}(AS_1)$$

$$S_3 = AS_2 + a_2 I_n \rightarrow AS_3 \quad a_3 = -\text{trace}(AS_2)$$

$$S_{n-1} = AS_{n-2} + a_{n-2} I_n \rightarrow AS_{n-1} \quad a_{n-1} = -\text{trace}(AS_{n-1})$$

$$S_n = AS_{n-1} + a_{n-1} I_n \rightarrow AS_n \quad a_n = S_n - \text{trace}(AS_n)$$

$$(SI-A)^{-1} = \frac{S_1 S^{n-1} + S_2 S^{n-2} + \dots + S_{n-1} S + S_n}{S^n + a_1 S^{n-1} + \dots + a_n}$$

$$\text{Note } S_{n+1} = AS_n + a_n I_n = 0$$

can be used as a check, if

you don't get zero at S_{n+1}

you know you fucked up somewhere.

$$S_1 = I_n$$

$$S_2 = AS_1 + a_1 I_n$$

$$S_3 = AS_2 + a_2 I_n$$

$$S_n = AS_{n-1} + a_{n-1} I_n$$

$$S_{n+1} = AS_n + a_n I_n$$

$$I_n$$

$$A + a_1 I_n$$

$$A^2 + a_1 A + a_2 I_n$$

$$A^3 + a_1 A^2 + a_2 A + a_3 I_n$$

$$S_{n+1} = A^n + a_1 A^{n-1} + a_2 A^{n-2} + \dots + a_{n-1} A + a_n I_n = 0$$

$$S^n + a_{n-1} S + a_n$$

$$S \rightarrow A$$

back to example.

$$\begin{pmatrix} 0 & -1 & -5-6 \\ 2 & 5 & 7 \\ 8+3 & 3 & 3 \end{pmatrix}$$

$$S_1 = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$a_1 = -\text{trace}(AS_1)/1$$

$$= -\text{trace} \begin{pmatrix} 9-6 & 0 & 0 \\ 0 & 5 & 0 \\ 0 & 0 & 3 \end{pmatrix}$$

$$a_1 = -5(9-6)(9+3)$$

For $n \times n$ matrix
 3×3

$$S'_1 = I$$

$$S'_2 = A + a_1 I$$

$$S'_3 = A^2 + a_1 A + a_2 I$$

$$\begin{pmatrix} 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

part 1

part 2

part 3

part 4

part 5

part 6

part 7

part 8

part 9

part 10

part 11

part 12

part 13

part 14

part 15

part 16

part 17

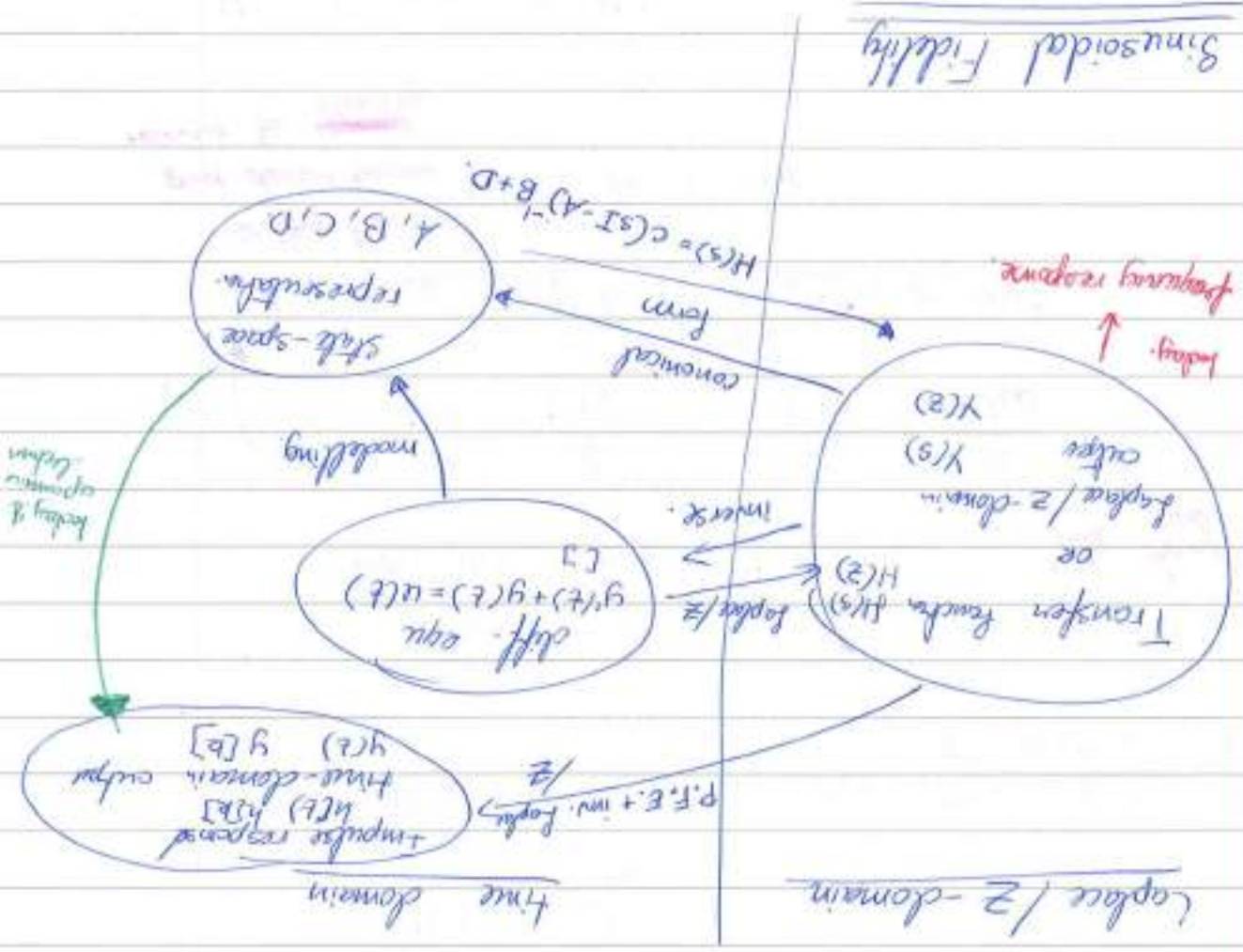
part 18

part 19

part 20

Mathematical Modelling

leave $\neq$ Sinusoidal Fidelity.



Sinusoidal Fidelity



$$u(t) = \begin{cases} \sin(\omega t) \\ \cos(\omega t) \\ e^{j\omega t} = \cos(\omega t) + j\sin(\omega t) \end{cases}$$

ω angular frequency (Rad/s)
 $\omega = \frac{1}{T} = \frac{2\pi}{T}$

$T = \frac{2\pi}{\omega}$ period.

What is the output for a stable system in steady-state?

$$Y(s) = H(s) U(s)$$

$$u(t) = e^{i\omega t}$$

$$e^{i\omega t} \xrightarrow{\mathcal{L}} \frac{1}{s-i\omega}$$

$$U(s) = \frac{1}{s-i\omega}$$

$$Y(s) = H(s) U(s) = \frac{b(s)}{a(s)} U(s) = \frac{b_0 s^n + b_1 s^{n-1} + \dots + b_n}{s^n + a_1 s^{n-1} + \dots + a_n} \frac{1}{s-i\omega}$$

$$= \frac{b(s)}{(s-p_1)(s-p_2)\dots(s-p_n)} \cdot \frac{1}{s-i\omega}$$

$\operatorname{Re}\{p_k\} < 0 \quad \forall k$
 real part of all poles is negative

$$\mathcal{L}^{-1} \left\{ Y(s) = \frac{A_1}{s-p_1} + \frac{A_2}{s-p_2} + \dots + \frac{A_n}{s-p_n} + \frac{B}{s-i\omega} \right\}$$

$$y(t) = A_1 e^{p_1 t} + A_2 e^{p_2 t} + \dots + A_n e^{p_n t} + B e^{i\omega t}$$

so then these

poles don't become relevant for ~~stability~~ stability $\Rightarrow 0$ for $t \rightarrow \infty$

How to compute B?

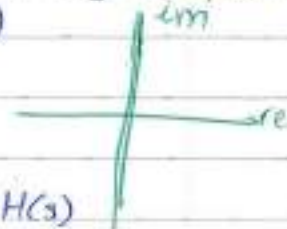
$$Y(s) (s-i\omega) \Big|_{s=i\omega} = \frac{A_1 (s-i\omega)}{s-p_1} \Big|_{s=i\omega} + \frac{A_2 (s-i\omega)}{s-p_2} \Big|_{s=i\omega} + \dots + \frac{A_n (s-i\omega)}{s-p_n} \Big|_{s=i\omega} + B$$

$$B = Y(s) (s-i\omega) \Big|_{s=i\omega}$$

$$B = H(s) U(s) (s-i\omega) \Big|_{s=i\omega}$$

$$= H(s) \frac{1}{s-i\omega} (s-i\omega) \Big|_{s=i\omega} = H(i\omega)$$

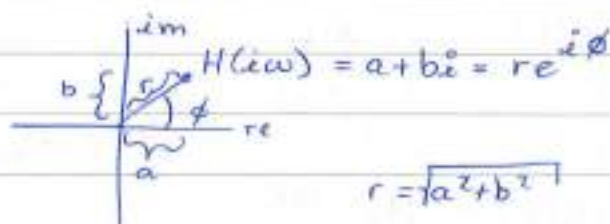
frequency response



$$h(t) \xrightarrow{\mathcal{L}} \int_0^\infty e^{-st} h(t) dt = H(s)$$

$$h(t) \xrightarrow{\mathcal{F}} \int_{-\infty}^\infty e^{-i\omega t} h(t) dt = H(\omega) = H(i\omega)$$

Input - $u(t) = e^{i\omega t}$
 steady-state output $y_s(t) = H(i\omega) e^{i\omega t}$



$$y_s(t) = re^{i\phi} e^{i\omega t}$$

$$= (re^{i(\omega t + \phi)})$$

$$= |H(i\omega)| e^{i(\omega t + \angle H(i\omega))}$$

$$\phi = \text{atan2}(b, a)$$

$$= \begin{cases} \arctan(b/a) & \text{if } a > 0 \\ \arctan(b/a) + \pi & \text{if } a < 0 \text{ and } b \geq 0 \\ \arctan(b/a) - \pi & \text{if } a < 0 \text{ and } b < 0 \\ \arctan(\pi/2) & \text{if } a = 0 \text{ and } b > 0 \\ -\pi/2 & \text{if } a = 0 \text{ and } b < 0 \\ \text{undefined} & \text{if } a = 0 \text{ and } b = 0. \end{cases}$$

exercise 22

$$H(s) = \frac{s^2 - 3s + 2}{s^2 + 4s + 3}$$

$$u(t) = 5 \cos(\omega t)$$

$\uparrow$
 $\omega = 3$

$$y_s(t) = 5 |H(3i)| (\cos(3t) + \angle H(3i))$$

$$y_s(t) = 5 (0.85) \cdot \cos(3t + 2.0169)$$

$$y_s(t) = 4.25 \cos(3t + 2.0169)$$

$$H(3i) = \frac{-9 - 9i + 2}{-9 + 12i + 3}$$

put 3i into H(s)

$$= \frac{-7 - 9i}{-6 + 12i} \cdot \frac{-1 - 2i}{-1 - 2i}$$

multiply by complex conjugate

$$= \frac{7 + 9i + 14i - 18}{6 - 12i + 12i + 24}$$

$$= \frac{-11 + 23i}{30}$$

$$\angle \frac{-11 + 23i}{30} = \text{atan2}\left(\frac{23}{30}, \frac{-11}{30}\right)$$

$$= \text{atan2}(23, -11)$$

$$= \arctan(23, -11) + \pi \approx 2.0169$$

$$|H(3i)| = \sqrt{\left(\frac{-11}{30}\right)^2 + \left(\frac{23}{30}\right)^2}$$

$$= \sqrt{\frac{13}{18}} \approx 0.85$$

Discrete-time sinusoidal Fidelity

$$u[k] = e^{i\Omega k} = \cos(\Omega k) + i \sin(\Omega k)$$

$\downarrow$

$$u(z) = \frac{z}{z - e^{i\Omega}}$$

$$H(z) = \frac{b(z)}{a(z)} = \frac{b(z)}{(z - p_1)(z - p_2) \dots (z - p_n)}$$

$$Y(z) = H(z)U(z) = \frac{zA_1}{(z-p_1)} + \frac{zA_2}{(z-p_2)} + \dots + \frac{zA_n}{(z-p_n)} + zB$$

become $\frac{z}{z-p_i}$ $\rightarrow$ $\frac{1}{1-p_i z^{-1}}$

$$y[k] = A_0 s[k] + A_1 (p_1)^k + A_2 (p_2)^k + \dots + A_n (p_n)^k + B e^{i\omega k}$$

if stable system, $\Rightarrow 0$ for $k > \infty$

$$y_s[k] = B e^{i\omega k}$$

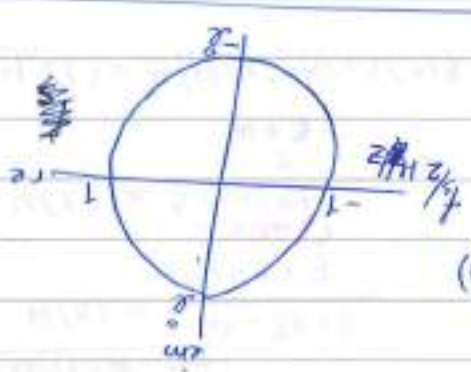
$$Y(z) = \frac{zB}{z - e^{i\omega}}$$

$$H(z)U(z) = \frac{zB}{z - e^{i\omega}} = \frac{zB}{z - e^{i\omega}}$$

$$B = H(z) \cdot \frac{1}{z - e^{i\omega}} \cdot (z - e^{i\omega}) \Big|_{z = e^{i\omega}}$$

$$B = H(e^{i\omega})$$

steady-state output
discrete time
 $y_s[k] = |H(e^{i\omega})| e^{i(k\omega + \angle H(e^{i\omega}))}$



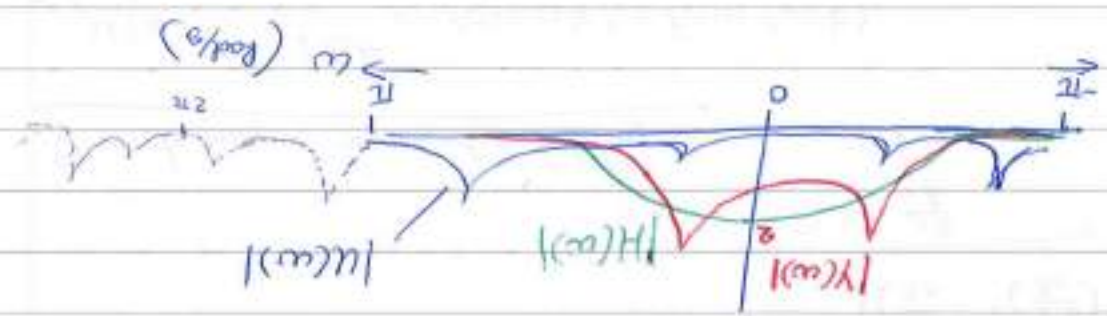
$$Y(s) = H(s)U(s)$$

$$Y(\omega) = H(\omega)U(\omega)$$

How to do filtering.

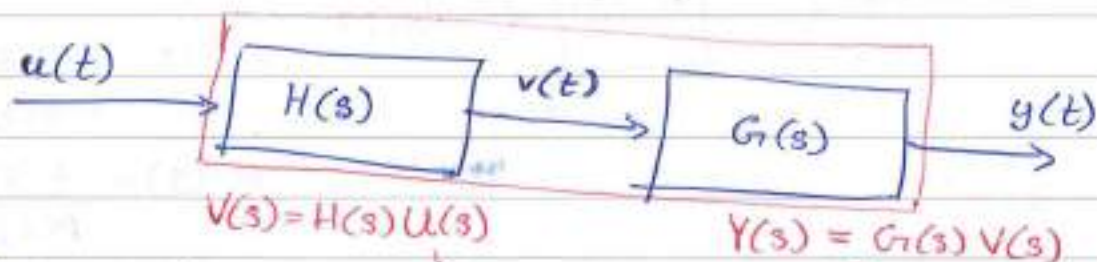
$$U(s) = \int_{-\infty}^{\infty} u(t) e^{-st} dt$$

$$U(\omega) = U(s) = \int_{-\infty}^{\infty} u(t) e^{-i\omega t} dt$$

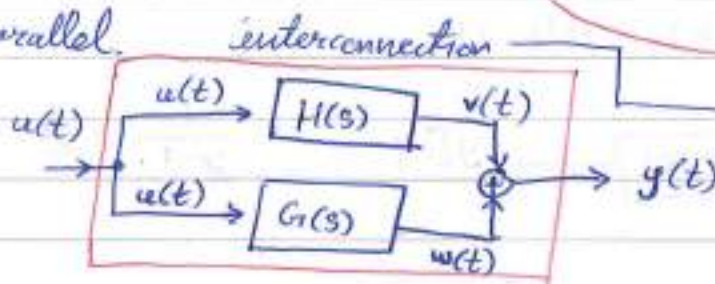


MM Lecture 8 - Interconnected Systems

- series / cascade interconnection



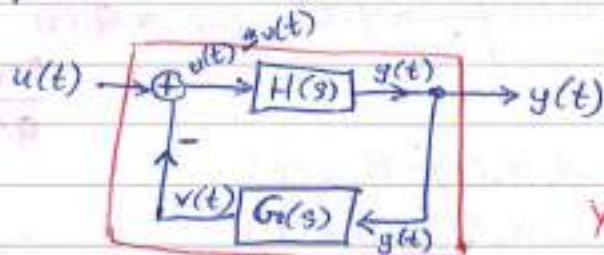
- parallel



$Y(s) = \boxed{G(s)H(s)} U(s)$
 t.p. of overall system

$V(s) = H(s)U(s)$
 $W(s) = G(s)U(s)$
 $Y(s) = V(s) + W(s)$

- feedback interconnection



$Y(s) = H(s)(U(s) - V(s))$

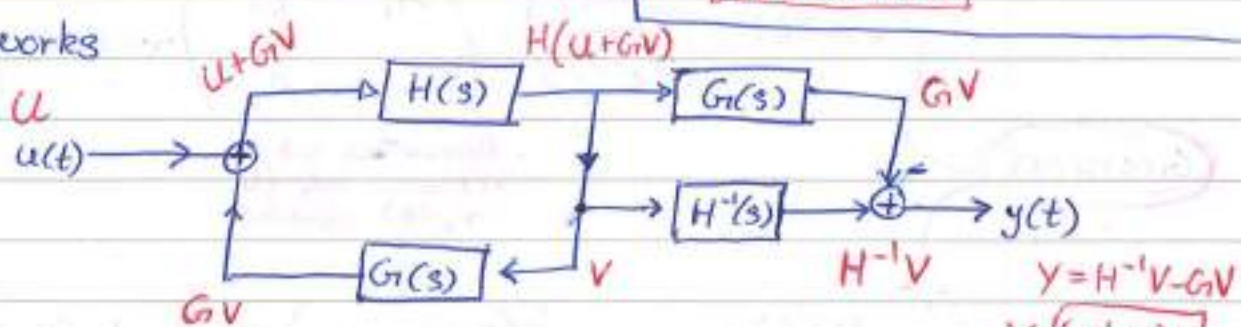
$V(s) = G(s)Y(s)$

$Y(s) = H(s)(U(s) - G(s)Y(s))$

$(1 + H(s)G(s))Y(s) = H(s)U(s)$

$Y(s) = \boxed{\frac{H(s)}{1 + H(s)G(s)}} \cdot U(s)$

- networks



$V = H(U + Gv)$

$V - HGv = HU$

$(1 - HG)v = HU$

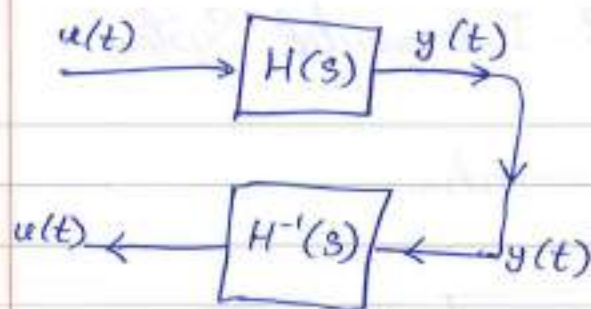
$V = \boxed{\frac{H}{1 - HG}} \cdot U$

$Y = H^{-1}V - Gv$
 $Y = \boxed{\frac{H^{-1}H}{1 - HG}} U$

$\frac{1 - Gv}{1 - HG} = 1$

so by chance

$Y = U$



inverse transfer function.

$$H^{-1}(s) = \frac{1}{H(s)}$$

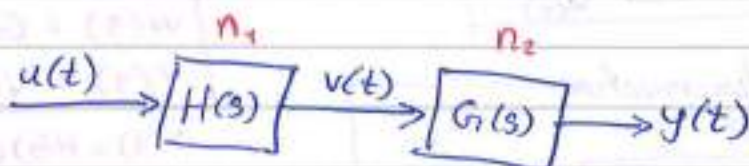
$$H(s) = \frac{P(s)}{Q(s)}$$

$$H^{-1}(s) = \frac{Q(s)}{P(s)}$$

$$y[k] = u[k-1]$$



$$\frac{1}{z^{-1}} = z \quad \frac{z}{1}$$



$$H(s) = \frac{P_1(s)}{Q_1(s)} \quad G(s) = \frac{P_2(s)}{Q_2(s)}$$

$$G(s)H(s) = \frac{P_1(s)P_2(s)}{Q_1(s)Q_2(s)}$$

$$H(s): \quad \begin{aligned} x_1'(t) &= A_1 x_1(t) + B_1 u(t) \\ v(t) &= C_1 x_1(t) + D_1 u(t) \end{aligned}$$

$$G(s): \quad \begin{aligned} x_2'(t) &= A_2 x_2(t) + B_2 v(t) \\ y(t) &= C_2 x_2(t) + D_2 v(t) \end{aligned}$$

$$x(t) = \begin{pmatrix} x_1(t) \\ x_2(t) \end{pmatrix}$$

$$x'(t) = \begin{pmatrix} x_1'(t) \\ x_2'(t) \end{pmatrix} = \begin{pmatrix} A_1 & 0 \\ B_2 C_1 & A_2 \end{pmatrix} x(t) + \begin{pmatrix} B_1 \\ B_2 D_1 \end{pmatrix} u(t)$$

because we sub
v(t) = ... into the
x_2'(t) equation.

$$y(t) = \begin{pmatrix} D_2 C_1 & C_2 \end{pmatrix} x(t) + \begin{pmatrix} D_2 D_1 \end{pmatrix} u(t)$$

order $\leq n_1 + n_2$

(need to cancel
like terms in
transfer func.)

here to scale the leading coefficient.

$$H(z) = C(zI - A)^{-1}B + D = \frac{D \det(zI - (A - BD^{-1}C))}{\det(zI - A)}$$

$$H^{-1}(z) = ? - D^{-1}C(zI - (A - BD^{-1}C))^{-1}BD^{-1} + D^{-1}$$

$$\begin{aligned} x[k+1] &= Ax[k] + Bu[k] \\ y[k] &= Cx[k] + Du[k] \end{aligned}$$

$$\begin{aligned} x[k+1] &= (A - BD^{-1}C)x[k] + (BD^{-1})y[k] \\ u[k] &= (-D^{-1}C)x[k] + (D^{-1})y[k] \end{aligned}$$

$$\frac{1}{D}y[k] - \frac{C}{D}x[k] = u[k]$$

$$x[k+1] = Ax[k] + B(-D^{-1}Cx[k] + D^{-1}y[k])$$

Solving State Equations

$$\begin{aligned} x'(t) &= Ax(t) + Bu(t) \\ x(t) &=? \end{aligned} \quad x(0) = x_0$$

$$\begin{aligned} x[k+1] &= Ax[k] + Bu[k] \\ x[k] &=? \end{aligned} \quad x[0] = x_0$$

$$x[0] = x_0$$

$$x[1] = Ax_0 + Bu[0]$$

$$x[2] = A^2x_0 + ABu[0] + Bu[1]$$

$$x[3] = A^3x_0 + A^2Bu[0] + ABu[1] + Bu[2]$$

$$x[k] = A^k x_0 + \sum_{l=0}^{k-1} A^{k-1-l} Bu[l]$$

$$y[k] = Cx[k] + Du[k]$$

$$y[k] = CA^k x_0 + \sum_{l=0}^{k-1} CA^{k-1-l} Bu[l] + Du[k]$$

$$h[k] = \begin{cases} D & k=0 \\ CA^{k-1}B & k>0 \end{cases} \quad \text{impulse response}$$

$$\boxed{x'(t) = Ax(t)}$$

$$x(0) = x_0$$

$$\dot{x} = ax$$

$$x(0) = x_0$$

$$x(t) = e^{at} x_0$$

$$\boxed{x(t) = e^{At} x_0}$$

Matrix exponential

$$e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots$$

$$e^M = I + M + \frac{M^2}{2!} + \frac{M^3}{3!} + \dots$$

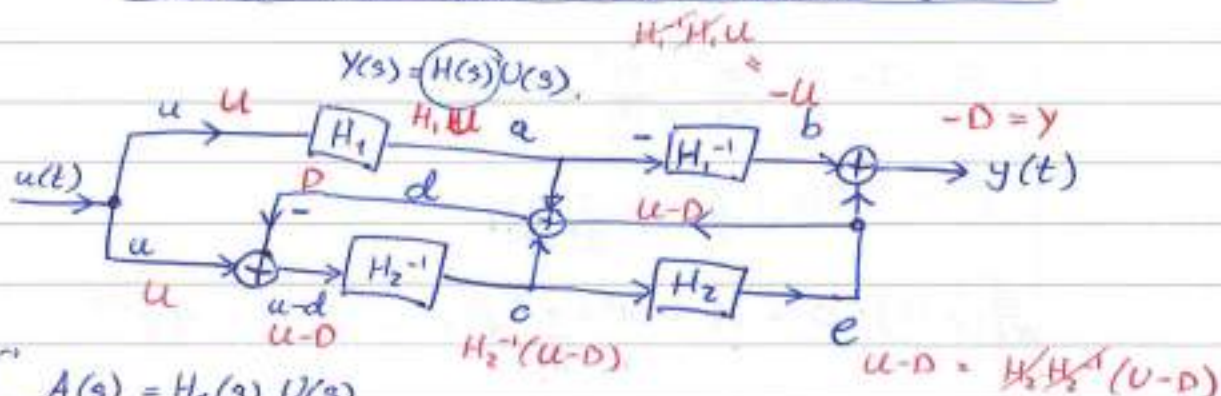
$$\begin{aligned} \frac{d}{dt}(e^{At} x_0) &= A e^{At} x_0 \\ &= A x(t) \end{aligned}$$

$$e^{At} = I + tA + \frac{t^2}{2!} A^2 + \frac{t^3}{3!} A^3 + \dots$$

$$\frac{d}{dt}(e^{At}) = 0 + A + tA^2 + \frac{t^2}{2!} A^3 + \dots = A(e^{At}) = e^{At} \cdot A$$

Discrete-time equivalents of continuous systems.

Ex. 21
Q4.



simple way

$$\begin{cases} A(s) = H_1(s) U(s) \\ B(s) = H_1^{-1}(s) (-A(s)) \\ C(s) = H_2(s)^{-1} (U(s) - D(s)) \\ E(s) = H_2(s) (C(s)) \end{cases} \quad \begin{cases} Y(s) = B(s) + E(s) \\ D(s) = A(s) + C(s) + E(s) \end{cases}$$

quick way.

$$\begin{aligned} D &= H_1 U + U - D + H_2^{-1} (U - D) \\ D &= H_1 U + U - D + H_2^{-1} U - H_2^{-1} D \\ (2 + H_2^{-1}) D &= (H_1 + 1 + H_2^{-1}) U \\ Y = -D &= \frac{(H_1 + 1 + H_2^{-1}) U}{(2 + H_2^{-1})} \end{aligned}$$

this is gonna be our transfer func.

discrete-time

$$x[k+1] = Ax[k] + Bu[k]$$

$$x[0] = x_0$$

$$x[0] = x_0$$

$$x[1] = Ax_0 + Bu[0]$$

$$x[2] = A^2 x_0 + ABu[0] + Bu[1]$$

$$x[3] = A^3 x_0 + A^2 Bu[0] + ABu[1] + Bu[2]$$

!

$$x[k] = A^k x_0 + \sum_{l=0}^{k-1} A^{k-l-1} B u[l]$$

$$= A^k x_0 + \sum_{l=0}^{k-1} A^l B u[k-1-l]$$

same thing, different way of writing index value.

scalar.

$$x'(t) = ax(t)$$

$$x(0) = x_0$$

$$x(t) = e^{at} x_0$$

multi-variable

$$x'(t) = Ax(t)$$

$$x(0) = x_0$$

$$x(t) = e^{At} x_0$$

$$e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots$$

$$e^M = I + M + \frac{M^2}{2!} + \frac{M^3}{3!} + \dots$$

$$e^{At} = I + At + \frac{t^2}{2!} A^2 + \frac{t^3}{3!} A^3 + \dots$$

$$\frac{d}{dt}(e^{At}) = 0 + A + tA^2 + \frac{t^2}{2!} A^3 + \dots = Ae^{At}$$

$$\underline{x}'(t) = \frac{d}{dt}(e^{At} x_0) = Ae^{At} x_0 = A \cdot x(t)$$

$$x'(t) = Ax(t) + Bu(t) \quad x(0) = x_0$$

$$x(t) = e^{At} x_0 + \int_0^t e^{A(t-\tau)} Bu(\tau) d\tau$$

does it work?

$$x(t) = e^{At} x_0 + \int_0^t e^{At} Bu(t-\tau) d\tau$$

the current time we are integrating

$$x'(t) = Ae^{At} x_0 + e^{A(t-t)} Bu(t) \cdot 1 + \int_0^t Ae^{A(t-\tau)} Bu(\tau) d\tau$$

$$\frac{d}{dx} \left(\int_{a(x)}^{b(x)} f(x,t) dt \right) = f(x, b(x)) \cdot \frac{d}{dx} b(x) - f(x, a(x)) \cdot \frac{d}{dx} a(x) + \int_{a(x)}^{b(x)} \frac{\partial}{\partial x} f(x,t) dt$$

(we start at zero if and differentiate if zero ending)

Leibniz's Rule.

$$x'(t) = A \left(\underbrace{e^{At} x_0 + \int_0^t e^{A(t-\tau)} Bu(\tau) d\tau}_{x(t)} \right) + Bu(t)$$

$$x(t) = e^{At} x_0 + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

$$\begin{aligned} x(0) &= x_0 \\ x(t) &= A x(t) \\ y(t) &= C x(t) + D u(t) \end{aligned}$$

$$y(t) = C e^{At} x_0 + \int_0^t C e^{A(t-\tau)} B u(\tau) d\tau + D u(t)$$

impulse response $u(t) = \delta(t)$

$$x_0 = 0$$

$$h(t) = C e^{At} B + D \delta(t)$$

$\mathcal{L}$

$$H(s) = C(sI - A)^{-1} B + D$$

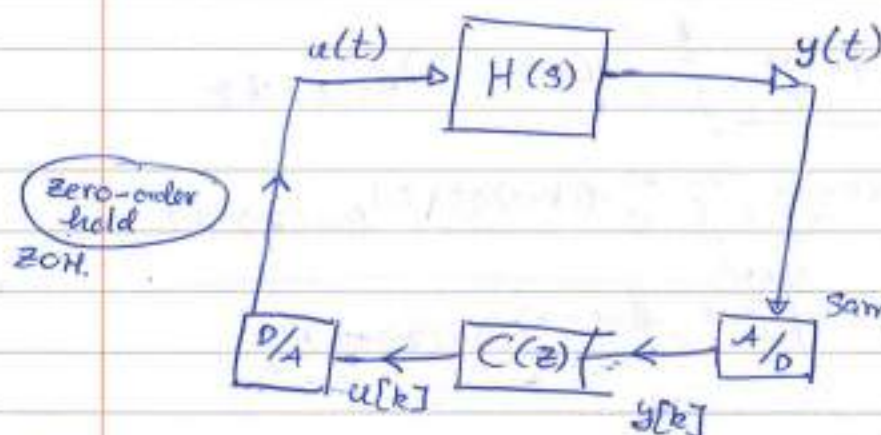
$$\int_0^\infty f(t) \delta(t) dt = f(0)$$

$$\mathcal{L}\{\delta(t)\} = 1$$

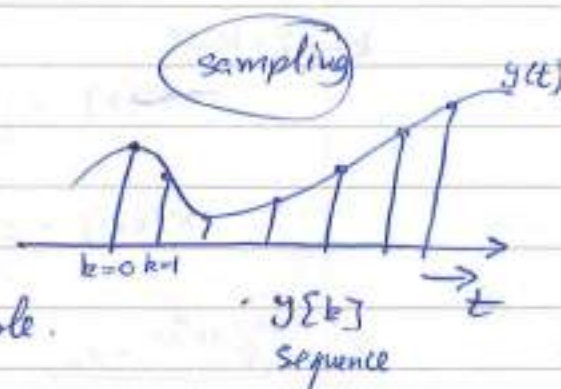
$$\mathcal{L}\{e^{at}\} = \frac{1}{s-a}$$

$$\frac{1}{s-a}$$

$$(sI - A)^{-1}$$

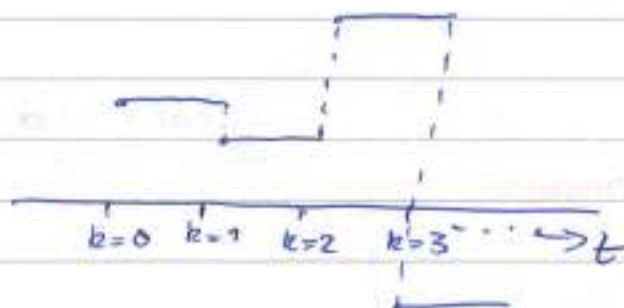


piecewise constant



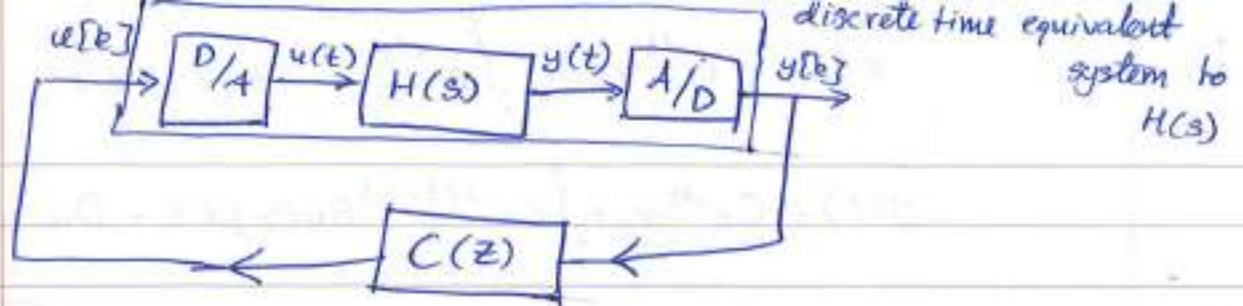
sampling interval Δt
 T_s T

ZOH interpretation



$$y[k] = y(k \cdot \Delta t)$$

$$u(t) = u[k] \text{ if } t \in [k \cdot \Delta t, (k+1) \Delta t)$$



continuous-time:

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$x(0) = x_0$$

$$y(t) = Cx(t) + Du(t)$$

at $k, t = k \cdot \Delta t$

$$u[k] = u(k \cdot \Delta t)$$

$$y[k] = y(k \cdot \Delta t)$$

$$x[k] = x(k \cdot \Delta t)$$

$$y[k] = Cx[k] + Du[k]$$

$$x(t) = e^{At} x_0 + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

$k \rightarrow t = k \cdot \Delta t$

$$x[k] = e^{A k \Delta t} x_0 + \int_0^{k \Delta t} e^{A(k \Delta t - \tau)} B u(\tau) d\tau$$

$$x[k+1] = e^{A(k+1)\Delta t} x_0 + \int_0^{(k+1)\Delta t} e^{A((k+1)\Delta t - \tau)} B u(\tau) d\tau$$

$$= e^{A \Delta t} e^{A k \Delta t} x_0 + \int_0^{k \Delta t} e^{A \Delta t} e^{A(k \Delta t - \tau)} B u(\tau) d\tau + \int_{k \Delta t}^{(k+1)\Delta t} e^{A((k+1)\Delta t - \tau)} B u(\tau) d\tau$$

$$= e^{A \Delta t} x[k] + \int_{k \Delta t}^{(k+1)\Delta t} e^{A((k+1)\Delta t - \tau)} B u(\tau) d\tau$$

$$= e^{A \Delta t} x[k] + \int_0^{\Delta t} e^{A(\Delta t - \tau)} B u(k \Delta t + \tau) d\tau$$

$u[k]$

$$x[k+1] = e^{A \Delta t} x[k] + \left(\int_0^{\Delta t} e^{A(\Delta t - \tau)} B d\tau \right) u[k]$$

Fixed matrix,
Fixed vector.

$$x[k+1] = \Phi x[k] + \Gamma u[k]$$

fixed matrix
 $e^{A \cdot \Delta t}$

fixed vector
 $\int_0^{\Delta t} e^{A(\Delta t - \tau)} d\tau$

$$= \int_0^{\Delta t} e^{A\tau'} d\tau'$$

$$\tau' = \Delta t - \tau$$

$$x'(t) = Ax(t) + Bu(t)$$

$$(A, B, C, D)$$

$\downarrow \Delta t$

$$\Rightarrow x[k+1] = \Phi x[k] + \Gamma u[k]$$

$$(A, B, C, D) \xrightarrow{\Delta t} (\Phi, \Gamma, C, D)$$

this equation shows what happens in the controller.

example.

$$\begin{cases} x'(t) = ax(t) \\ y(t) = x(t) \end{cases} \Rightarrow x(t) = e^{at} x_0$$

$$x[k] = x(k\Delta t) = e^{ak\Delta t} x_0 = (e^{a\Delta t})^k x_0$$

$$\begin{aligned} x[k+1] &= (e^{a\Delta t})^{k+1} x_0 = e^{a\Delta t} \cdot (e^{a\Delta t})^k x_0 \\ &= e^{a\Delta t} \cdot x[k] \end{aligned}$$

$$x[k+1] = e^{a\Delta t} x[k]$$

A

$$\Phi = e^{A\Delta t}$$

$$M \rightarrow e^M$$

$$\lambda_1, \lambda_2, \dots, \lambda_n \longrightarrow e^{\lambda_1 \Delta t}, e^{\lambda_2 \Delta t}, \dots, e^{\lambda_n \Delta t}$$

$$\lambda = a + bi; \quad |e^{\lambda \Delta t}| = |e^{a\Delta t}| \cdot \underbrace{|e^{bi\Delta t}|}_{=1} = e^{a\Delta t} < 1$$

$(a < 0)$

$$y = v + \epsilon$$

$$y = v + \epsilon \quad | \quad v \sim N(0, \sigma_v^2) \quad \epsilon \sim N(0, \sigma_\epsilon^2)$$

$$y = v + \epsilon$$

$$y = v + \epsilon \quad | \quad v \sim N(0, \sigma_v^2) \quad \epsilon \sim N(0, \sigma_\epsilon^2)$$

$$y = v + \epsilon$$

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$$y = v + \epsilon$$

Mathematical Modelling

Lecture 10

Pole-placement with state-feedback.

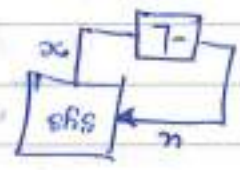


Can we automatically stabilize the system by choosing inputs using the state? Yes! with fixed linear combination of states. (provided controllable).

Recall.

controllable if $w_c = [B \ AB \ \dots \ A^{n-1}B]$ is non-singular (is invertible/determinant $\neq 0$).

$$u = -Lx = [-L_1 x_1, -L_2 x_2, \dots, -L_n x_n]$$



How to find L?

First for special case: sys in controllable canonical form.

CT

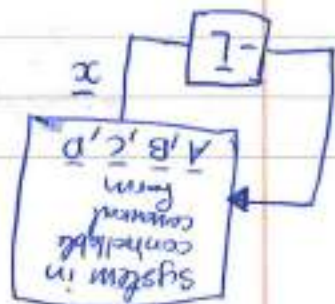
$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases}$$

DT

$$\begin{cases} x[k+1] = (A-BL)x[k] + Bu[k] \\ u[k] = -Lx[k] \end{cases}$$

sys matrix of closed loop.

$$(A-BL)x(t)$$



$$\bar{B} = \begin{pmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{pmatrix} \quad \bar{L} = [\bar{L}_1 \bar{L}_2 \dots \bar{L}_n]$$

$$\bar{A} = \begin{pmatrix} -a_1 & -a_2 & \dots & -a_n \\ & & I & \\ & & & \ddots \\ & & & 0 \end{pmatrix}$$

$$\text{Then } \bar{A} - \bar{B}\bar{L} = \begin{pmatrix} -a_1 & -a_2 & \dots & -a_n \\ & & I & \\ & & & \ddots \\ & & & 0 \end{pmatrix} - \begin{pmatrix} \bar{L}_1 \bar{L}_2 \dots \bar{L}_n \\ & & & \\ & & & \\ & & & 0 \end{pmatrix}$$

$$= \begin{pmatrix} -a_1 + \bar{L}_1 & -a_2 + \bar{L}_2 & \dots & -a_n + \bar{L}_n \\ & & I & \\ & & & \ddots \\ & & & 0 \end{pmatrix}$$

Characteristic polynomial (CP) of $\bar{A}$.

$$\det(sI - \bar{A}) = s^n + a_1 s^{n-1} + \dots + a_n$$

Poles of the system.

Roots of CP.

eigenvalues of $\bar{A}$

Poles $p_1, p_2, \dots, p_n$

$$\text{CP of } \bar{A} - \bar{B}\bar{L} : \det(sI - [\bar{A} - \bar{B}\bar{L}]) = s^n + (a_1 + \bar{L}_1)s^{n-1} + \dots + (a_n + \bar{L}_n)$$

desired pole locations of closed loop system are $\bar{p}_1, \bar{p}_2, \dots, \bar{p}_n$
 hence desired CP : $(s - \bar{p}_1)(s - \bar{p}_2) \dots (s - \bar{p}_n)$

$$= s^n + \bar{a}_1 s^{n-1} + \bar{a}_2 s^{n-2} + \dots + \bar{a}_n$$

hence we choose $\bar{L}_1 = \bar{a}_1 - a_1, \bar{L}_2 = \bar{a}_2 - a_2, \dots, \bar{L}_n = \bar{a}_n - a_n$

$$\bar{L} = (\bar{a}_1 - a_1, \bar{a}_2 - a_2, \dots, \bar{a}_n - a_n)$$

This is pole-placement.

What if the system is NOT in controllable canon. form?

- 1) pretend that it is in contr. canon. form and find $\bar{L}$.
- 2) find ss transformation T to bring it into controllable canonical form.
- 3) find the feedback law for the ss representation that we have.

$$\bar{A} = TAT^{-1}$$

$$\bar{x}(t) = Tx(t)$$

$$\bar{B} = TB$$

$$\bar{C} = CT^{-1}$$

$$\bar{D} = D$$

$$T^{-1} = W_c \bar{W}_c^{-1}$$

$$= (B \ AB \ \dots \ A^{n-1}B) \begin{pmatrix} 1 & a_1 & \dots & a_n \\ & 0 & \dots & a_1 \\ & & \ddots & 1 \end{pmatrix}$$

$$u(t) = -\bar{L}\bar{x}(t) = -\bar{L}Tx(t) = Lx(t)$$

$$\Rightarrow L = \bar{L}T$$

Ex.

$$\begin{cases} \dot{x}(t) = \begin{pmatrix} -2 & -2 & -\frac{3}{2} \\ 2 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix} x(t) + \begin{pmatrix} 2 \\ 0 \\ 0 \end{pmatrix} u(t) \\ y(t) = \begin{pmatrix} \frac{1}{2} & -\frac{1}{2} & \frac{3}{4} \end{pmatrix} x(t) \end{cases}$$

goal: all pole locations of closed-loop system at $s = -2$.

1) find $\bar{L}$

a) find CP

$$a(s) = \det(sI - A) = \det \begin{pmatrix} s+2 & 2 & 3/2 \\ -2 & s & 0 \\ 0 & -1 & s \end{pmatrix}$$

$$= s \det \begin{pmatrix} s+2 & 2 \\ -2 & s \end{pmatrix} + \det \begin{pmatrix} s+2 & 3/2 \\ -2 & 0 \end{pmatrix}$$

$$= s[(s+2)s + 4] + 3 = s^3 + 2s^2 + 4s + 3$$

$$a_0 = 1, a_1 = 2, a_2 = 4, a_3 = 3$$

b) find desired CP.

we want poles at $s = -2$.

$$(s+2)^3 = s^3 + 6s^2 + 12s + 8$$

$$\hat{a}_0 = 1, \hat{a}_1 = 6, \hat{a}_2 = 12, \hat{a}_3 = 8$$

c) find $\bar{L}$ $\bar{L}_1 = \hat{a}_1 - a_1 = 6 - 2 = 4$

$$\bar{L}_2 = \hat{a}_2 - a_2 = 12 - 4 = 8$$

$$\bar{L}_3 = \hat{a}_3 - a_3 = 8 - 3 = 5$$

$$\bar{L} = (4 \ 8 \ 5)$$

2) find T^{-1} and T .

$$W_c = (B \ AB \ A^2B)$$

$$= \begin{pmatrix} 2 & -4 & 0 \\ 0 & 4 & -8 \\ 0 & 0 & 4 \end{pmatrix}$$

$$\bar{W}_c^{-1} = \begin{pmatrix} 1 & a_1 & a_2 \\ 0 & 1 & a_1 \\ 0 & 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} 1 & 2 & 4 \\ 0 & 1 & 2 \\ 0 & 0 & 1 \end{pmatrix}$$

$$T^{-1} = W_c \bar{W}_c^{-1}$$

$$= \begin{pmatrix} 2 & -4 & 0 \\ 0 & 4 & -8 \\ 0 & 0 & 4 \end{pmatrix} \begin{pmatrix} 1 & 2 & 4 \\ 0 & 1 & 2 \\ 0 & 0 & 1 \end{pmatrix}$$

$$T^{-1} = \begin{pmatrix} 2 & 0 & 0 \\ 0 & 4 & 0 \\ 0 & 0 & 4 \end{pmatrix}$$

$$T = \begin{pmatrix} 1/2 & 0 & 0 \\ 0 & 1/4 & 0 \\ 0 & 0 & 1/4 \end{pmatrix}$$

3) $L = \bar{L}T$

$$= (4 \ 8 \ 5) \begin{pmatrix} 1/2 & 0 & 0 \\ 0 & 1/4 & 0 \\ 0 & 0 & 1/4 \end{pmatrix}$$

~~4 now~~ $= (2 \ 2 \ 5/4) = L$

$$x'(t) = \begin{pmatrix} -2 & -2 & -3/2 \\ 2 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix} x(t) + \underbrace{\begin{pmatrix} 2 \\ 0 \\ 0 \end{pmatrix} (2 \ 2 \ 5/4)}_{\text{produces } 3 \times 3 \text{ matrix}} x(t)$$

produces 3×3 matrix

you can then make one big 3×3 matrix

to show the closed loop state-space model for the system.

Controllability

$$\begin{aligned} x\{1\} &= Ax_0 + Bu\{0\} \\ x\{2\} &= Ax\{1\} + Bu\{1\} \\ &= A^2x_0 + ABu\{0\} + Bu\{1\} \end{aligned}$$

$$x\{n\} = A^n x_0 + A^{n-1}Bu\{0\} + \dots + Bu\{n-1\}$$

$W_c = (b \mid Ab \mid \dots \mid A^{n-1}b)$
 (this like everything in the system for the state but in reverse order.)
 remove all column vectors of length n
 controllability matrix.

input as vector $\tilde{u} = \begin{pmatrix} u\{0\} \\ \vdots \\ u\{n-1\} \end{pmatrix}$

$$x\{n\} = A^n x_0 + W_c \tilde{u}$$

$$x\{n\} = A^n x_0 + W_c \tilde{u}$$

$$x\{n\} - A^n x_0 = W_c \tilde{u} \Rightarrow \tilde{u} = W_c^{-1} (x\{n\} - A^n x_0)$$

we can go from x_0 to x_n by using input $\tilde{u}$ if W_c^{-1} exists.

If W_c^{-1} is invertible, we can bring the system from x_0 to x_n using the input.

Observability

$$\begin{aligned} x\{k+1\} &= Ax\{k\} + Bu\{k\} \\ y\{k\} &= Cx\{k\} + du\{k\} \end{aligned}$$

can't prove to make it easier.

$$\begin{aligned} y\{0\} &= Cx_0 \\ y\{1\} &= Cx\{1\} = CAx_0 \\ y\{2\} &= Cx\{2\} = CA^2x_0 \\ &\vdots \\ y\{n-1\} &= Cx\{n-1\} = CA^{n-1}x_0 \end{aligned}$$

$$y[n-1] = cA^{n-1}x_0$$

$$y = \begin{pmatrix} y[0] \\ y[1] \\ \vdots \\ y[n-1] \end{pmatrix}$$

observability matrix

$$W_o = \begin{pmatrix} c \\ cA \\ \vdots \\ cA^{n-1} \end{pmatrix}$$

$$y = W_o x_0$$

$$\Rightarrow x_0 = W_o^{-1} y$$

we can see the state x_0 from the output by multiplying it w/ W_o^{-1} .

Minimality.

- Minimal if system is both controllable and observable.
- Non-minimal systems will have pole-zero cancellation in the transfer function.
- Effectively low-order if minimal system.

Controllable Canonical Form.

Recall Canonical Form:

in state-space $n^2 + 2n + 1$ parameters

in transfer-func $2n + 1$ parameters ~~is~~ with ~~canonical form~~ ~~is~~ state-space ~~2n+1~~ ~~param~~
going from tf to ~~ss~~ canonical form is easy
just plug in a's and b's.

controllable canonical form. $y[k] = (b_1 - a_1b_0 \quad b_2 - a_2b_0 \quad \dots \quad b_n - a_nb_0) \tilde{x}[k] + b_0u[k]$

$$\tilde{x}[k+1] = \begin{pmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & 1 & 0 \end{pmatrix} \tilde{x}[k] + \begin{pmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{pmatrix} u[k]$$

$$\bar{x}[k+1] = \begin{pmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & 1 & 0 \end{pmatrix} \bar{x}[k] + \begin{pmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{pmatrix} u[k]$$

$\bar{x}[k] = \begin{pmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{pmatrix} u[k]$

$$\bar{W}_c = (\bar{b} \mid \bar{A}\bar{b} \mid \dots \mid \bar{A}^{n-1}\bar{b})$$

selects first column of A as our b is just

$$\begin{pmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{pmatrix}$$

the '-' is to indicate then a system in controllable canonical form.

$$= \begin{pmatrix} 1 & -a_1 & a_1^2 - a_2 & -a_1^3 + 2a_1a_2 + a_3 & \dots \\ 0 & 1 & -a_1 & a_1^2 - a_2 & \dots \\ \vdots & 0 & 1 & -a_1 & \dots \\ \vdots & \vdots & \vdots & 1 & \dots \\ 0 & 0 & 0 & \dots & 1 \end{pmatrix}$$

but this shit is ugly (no better, so let's do something easier)

first column is just b

$$\bar{W}_c^{-1} = \begin{pmatrix} 1 & a_1 & a_2 & \dots & a_{n-1} \\ 0 & \ddots & \ddots & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & a_2 \\ \vdots & \ddots & \ddots & \ddots & a_1 \\ 0 & \dots & \dots & 0 & 1 \end{pmatrix}$$

$$A^2b = A^*Ab$$

$$= A^* \begin{pmatrix} -a_1 \\ 1 \\ 0 \\ \vdots \\ 0 \end{pmatrix} = -a_1 \times -a_1 + 1 \times a_1 = a_1^2 - a_2$$

$$= A^* \begin{pmatrix} -a_1 \\ 1 \\ 0 \\ \vdots \\ 0 \end{pmatrix} = -a_1 \times -a_1 + 1 \times a_1 = a_1^2 - a_2$$

$$\bar{A} = TAT^{-1}, \bar{b} = Tb, \bar{c} = cT^{-1}, \bar{d} = d, \bar{x}[k] = Tx[k]$$

→ But we need to find an appropriate T .

$$\bar{W}_c = (\bar{b} \mid \bar{A}\bar{b} \mid \bar{A}^2\bar{b} \mid \dots \mid \bar{A}^{n-1}\bar{b})$$

this is in controllable canonical form

$$= (Tb \mid TAT^{-1}Tb \mid TAT^{-1}TA^{-1}Tb \mid \dots \mid TAT^{-1}TA^{-1} \dots TA^{-1}Tb)$$

$$= (Tb \mid TAB \mid TA^2b \mid \dots \mid TA^{n-1}b)$$

$$= TW_c$$

we know this

hard to find anyway

$$\bar{W}_c = TW_c \Rightarrow \bar{W}_c W_c^{-1} = T$$

easy to find easy piece to find

$$T^{-1} = W_c \bar{W}_c^{-1}$$

Ex.

$$x'(t) = \begin{pmatrix} 1 & 3 & -1 \\ 2 & -1 & -1 \\ 0 & 0 & 3 \end{pmatrix} x(t) + \begin{pmatrix} 8 \\ 1 \\ 0 \\ -1 \end{pmatrix} u(t)$$

$$T^{-1} = W_c \bar{W}_c^{-1}$$

$$W_c = (B \quad AB \quad A^2B) = \begin{pmatrix} 1 & 2 & 14 \\ 0 & 3 & 4 \\ -1 & -3 & -9 \end{pmatrix}$$

$$\bar{W}_c^{-1} = \begin{pmatrix} 1 & a_1 & a_2 \\ 0 & 1 & a_1 \\ 0 & 0 & 1 \end{pmatrix}$$

find characteristic polynomial.

$$a(s) = \det(sI - A) = \det \begin{pmatrix} s-1 & -3 & 1 \\ -2 & s+1 & 1 \\ 0 & 0 & s-3 \end{pmatrix}$$

$$= (s-3) \det \begin{pmatrix} s-1 & -3 \\ -2 & s+1 \end{pmatrix}$$

$$= (s-3) [(s-1)(s+1) - (-2)(-3)]$$

$$= (s-3)(s^2 - 7)$$

$$= s^3 - 3s^2 - 7s + 21$$

$$a_0 = 1, a_1 = -3, a_2 = -7, a_3 = 21$$

$$\bar{W}_c^{-1} = \begin{pmatrix} 1 & -3 & -7 \\ 0 & 1 & -3 \\ 0 & 0 & 1 \end{pmatrix}$$

$$T^{-1} = W_c \bar{W}_c^{-1} = \begin{pmatrix} 1 & 2 & 14 \\ 0 & 3 & 4 \\ -1 & -3 & -9 \end{pmatrix} \begin{pmatrix} 1 & -3 & -7 \\ 0 & 1 & -3 \\ 0 & 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} 1 & -1 & 1 \\ 0 & 3 & -5 \\ -1 & 0 & 7 \end{pmatrix}$$

$$T = \begin{pmatrix} \frac{21}{19} & \frac{21}{57} & \frac{2}{19} \\ \frac{3}{19} & \frac{24}{57} & \frac{5}{19} \\ \frac{3}{19} & \frac{1}{19} & \frac{3}{19} \end{pmatrix}$$

$$\left(\begin{array}{ccc|ccc} 1 & -1 & 1 & 1 & 0 & 0 \\ 0 & 3 & -5 & 0 & 1 & 0 \\ -1 & 0 & 7 & 0 & 0 & 1 \end{array} \right) \sim \left(\begin{array}{ccc|ccc} 1 & 0 & -2/3 & 1 & 1/3 & 0 \\ 0 & 1 & -5/3 & 0 & 1/3 & 0 \\ 0 & -1 & 8 & 1 & 0 & 1 \end{array} \right)$$

2/4